

5-1995

Final Specification Report for the AISC Steel Bridge Design for the AISC Bridge-Building Competition c/o Egyptian Associates

Derek A. Peebles

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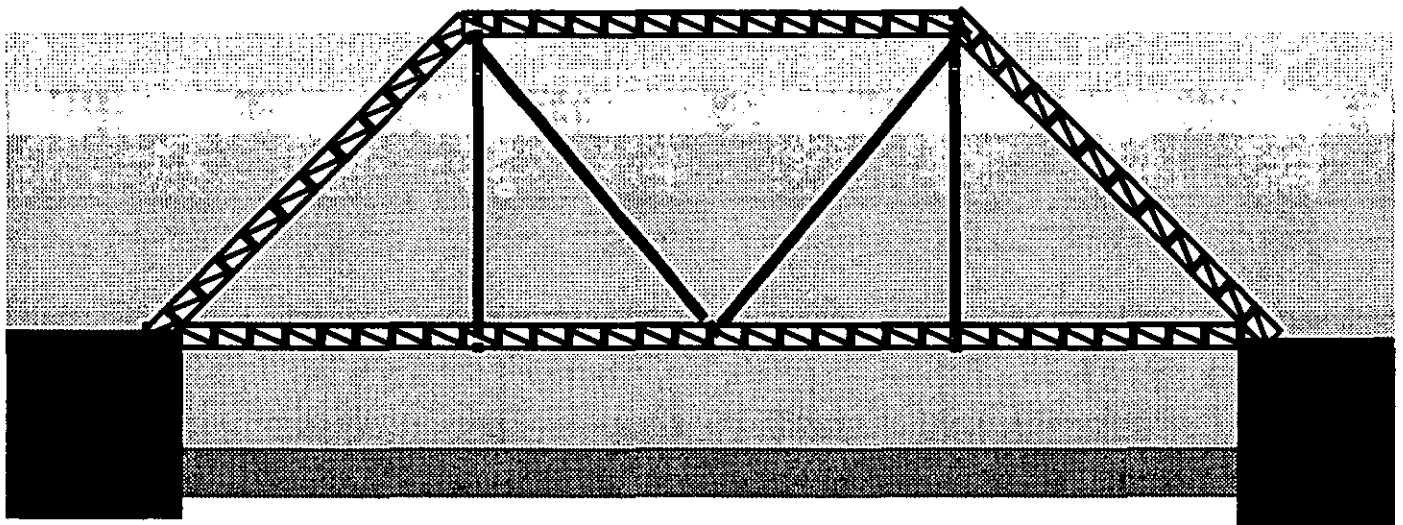
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**FINAL SPECIFICATION REPORT
FOR**

**THE AISC
STEEL BRIDGE
DESIGN**

**FOR
AISC BRIDGE-BUILDING COMPETITION
c/o EGYPTIAN ASSOCIATES**



**PREPARED
BY**

**SALUKI ENGINEERING COMPANY
GROUP VI**

**EA REFERENCE NO. BRIDGE06.S95
SEC REFERENCE NO. DES.06.S95**

APRIL 26, 1995

May 5, 1995

Dr. Williams:

With this letter, you will find the completed design report for my Honors Thesis Project. As I have mentioned, the design was undertaken by myself and two other senior engineering students, under the supervision of an advisor.

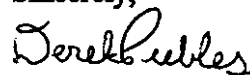
To give you a little background about the nature of bridge design, it was preformed with the intention of entering the bridge in the 1996 AISC (American Institute of Steel Construction) Steel Bridge Competition. The regional and national competitions are sponsored annually by AISC, giving civil engineering students an opportunity to apply their text book knowledge with the design and construction of a 1:10 scale steel bridge. The rules of the competition are quite extensive and meant to replicate the challenges of an actual bridge project. I have included a copy of the 1995 rules in the back pocket of the design notebook.

The Southern Illinois University at Carbondale Chapter of The American Society of Civil Engineers (ASCE) has participated in the bridge competition for three years running, becoming more competitive with each passing year. This past year the chapter's bridge won in the category of lightest bridge at the Regional competition held at Kansas State University. We have incorporated lessons learned from the past bridge designs and believe that this currently completed design has the necessary compromise between weight, stiffness, and speed of assembly, to enable it to win in the overall category at next year's competition.

I must mention that this report is a summary of the design procedure which will be followed by the team of ASCE members who will fabricate the bridge in the Fall of 1995. For this reason, it does not include the large bulk of calculations and other work which resulted in the final design.

As a final note, I wish to thank you and everyone else who has contributed their time and energy into making the Honors Program at SIUC such success. It has truly enriched my experiences at SIUC. In particular, I cannot say enough about the lecture series. The speakers which you have scheduled have been a constant source of new ideas and inspiration to me and I know many others. I will miss them when I leave SIUC. Keep up the good work and again thank you.

Sincerely,



Derek Peebles

Saluki Engineering Company
1200 South Illinois Avenue
Carbondale, IL 62901
April 26, 1995

Kay Purcell
Manager of Projects
Egyptian Associates
1000 Douglas Drive
Carbondale, IL 62901-6603

Subject: Final Report for design of steel bridge
Project No: BRIDGE06.S95
SEC No: DES06.S95

Dear Mrs. Purcell:

This letter is to inform you that the eleven week study and design of the AISC Steel Bridge has been completed as contracted. Saluki Engineering Company hereby submits the AISC Steel Bridge design specification report to Egyptian Associates at 12:00 pm on April 26, 1995.

Saluki Engineering Company would like to thank you for the opportunity to work on this design project. If you have any questions regarding this report, please contact the project manager, Sarah Ohler, at (618) 529-4252.

Sincerely,

Bill DeBridge
Vice President
Saluki Engineering Company

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EXECUTIVE SUMMARY

The Steel Bridge has been completed in accordance with the request for proposal received on January 31, 1995 from Egyptian Associates. Included in the report is a detailed drawing of each member and each connection, a fabrication sequence, an assembly sequence, a final analysis of the design, a cost summary, and a critical path schedule and PERT chart.

The bridge for the 1996 AISC National Steel Bridge Competition has been designed for stiffness, lightness, construction speed, aesthetics, efficiency, and economy. Its height and basic structural design encompass the stiffness aspect. The economy and lightness are due to the type of steel members used. Hinged members allow for the efficiency and speed in construction. Aesthetics were incorporated into the design and painting of the bridge.

The bridge will cost \$494.22 in steel, if nothing is donated, and \$835.34 in labor, if no time is volunteered. It will take 37 hours to fabricate for a 4 person crew, weigh approximately 125 lbs., and be able to be assembled in about 3 minutes. Volunteer time from members of ASCE will be used in fabrication and assembly processes.

CAPITAL COST SUMMARY

Materials:

Structural Steel Tubing:

Type	Length	Quantity	Cost/each	Vendor
1/2" x 1/2" x 0.049	3'	3	\$2.95	TVH
5/8" x 5/8" x 0.049	6'	8	\$6.90	TVH
1" x 1" x 0.049	6'	8	\$10.69	TVH
1 1/4" x 1 1/4" x 0.049	6'	8	\$12.59	TVH
1 1/4" x 1 1/4" x 0.083	6'	1	\$13.79	TVH
1 1/2" x 1 1/2" x 0.109	3'	1	\$12.18	M-C

Vendors:

TVH = True Value Hardware

M-C = McMaster - Carr Supply Company

Round UNC, class 2 Threaded Steel Rods:

Type	Length	Quantity	Cost/each	Vendor
1/4"	3'	8	\$0.96	TVH
1/4"	6'	4	\$1.92	TVH
3/8"	6'	2	\$1.20	TVH

Hook and Eye Steel Turnbuckles (UNC, class 2 threads):

Bolt Diameter	Quantity	Cost/each	Vendor
1/4"	8	\$4.92	M-C
3/8"	2	\$6.87	M-C

Dent Ring Pins:

Type	Quantity	Cost/each	Vendor
1/4" x 1 3/4"	40	\$2.00	TVH

CAPITAL COST SUMMARY (continued)

Elevator Bolts:

Type	Quantity	Cost/each	Vendor
1/4" x 2"	20	\$0.32	TVH

Eye Bolts:

Type	Quantity	Cost/each	Vendor
3/8" x 1 1/4"	9	\$1.11	M-C

Angle:

Type	Quantity	Cost/each	Vendor
1" x 1" x 1/8" x 5'	1	\$22.03	M-C

Acetone:

Type	Quantity	Cost/each	Vendor
generic	2	\$2.29/pint	TVH

Primer:

Type	Quantity	Cost/each	Vendor
X-O Rust	2	\$3.28/pint	TVH

Paint:

Type	Quantity	Cost/each	Vendor
Spray Enamel	4	\$1.09/12oz	TVH

Hinges:

Type	Quantity	Cost/each	Vendor
1" loose pin	8	\$2.55/2	TVH

CAPITAL SUMMARY COST (continued)

Lubricant:

Type	Quantity	Cost/each	Vendor
WD-40	2	\$1.49/6oz	TVH

TOTAL MATERIALS COST = \$494.22

Labor and equipment:

(Means Building Construction Cost Data)

Cutting:

$$\$12.95/\text{hour} * 6 \text{ hours} + \$20/\text{day} * 1 \text{ day} = \$97.70$$

Cleaning:

$$\$5.45/\text{hour} * 1.5 \text{ hours} = \$8.18$$

Drilling:

$$\$12.95/\text{hour} * 6 \text{ hours} + \$20/\text{day} * 1 \text{ day} = \$97.70$$

Welding:

$$\$37.88/\text{hour} * 14.5 \text{ hours} = \$549.26$$

Painting:

brush:

$$6 \text{ hours} * \$8.45/\text{hr} = \$50.70$$

spray:

$$4 \text{ hours} * \$7.95/\text{hr} = \$31.80$$

TOTAL LABOR AND EQUIPMENT COSTS = \$835.34

TOTAL COST = \$1,329.56

DESCRIPTION OF ACTIVITY CODES

Activity Code Name	Description	Duration (hrs)
A	Order the steel members and parts	14
B	Locate pick-up truck to pick up the steel	2
C	Secure permission and ID badges to use the workshop	2
D	Secure a welder for later in the fabrication	3
E	Pick up the steel	3
F	Measure and cut the steel to specified sizes	24
G	File the rough edges and wipe steel with cloth for safety and for a clean fit	2
H	Tack weld the connections, unless the connections are too awkward to fit the drill press.	22
I	Drill the holes. Align the connections while drilling.	22
J	File the edges of the holes for a good bolt or pin fit	2
K	Replace the tack welds with a strong, permanent weld	36
L	Assemble the bridge to check for any needed adjustments	8
M	Clean the entire bridge with acetone	4
N	Coat the bridge with primer	16
O	Paint the bridge while it is together to avoid any unwanted thickness on members needing to fit into sleeves	16
P	Stencil the school name on the bottom chord members	8
Q	Practice assembly several times to optimize the process	20
R	Assemble the bridge at the 1995 AISC Steel Bridge Competition	8

SCHEDULE TO FABRICATE THE BRIDGE

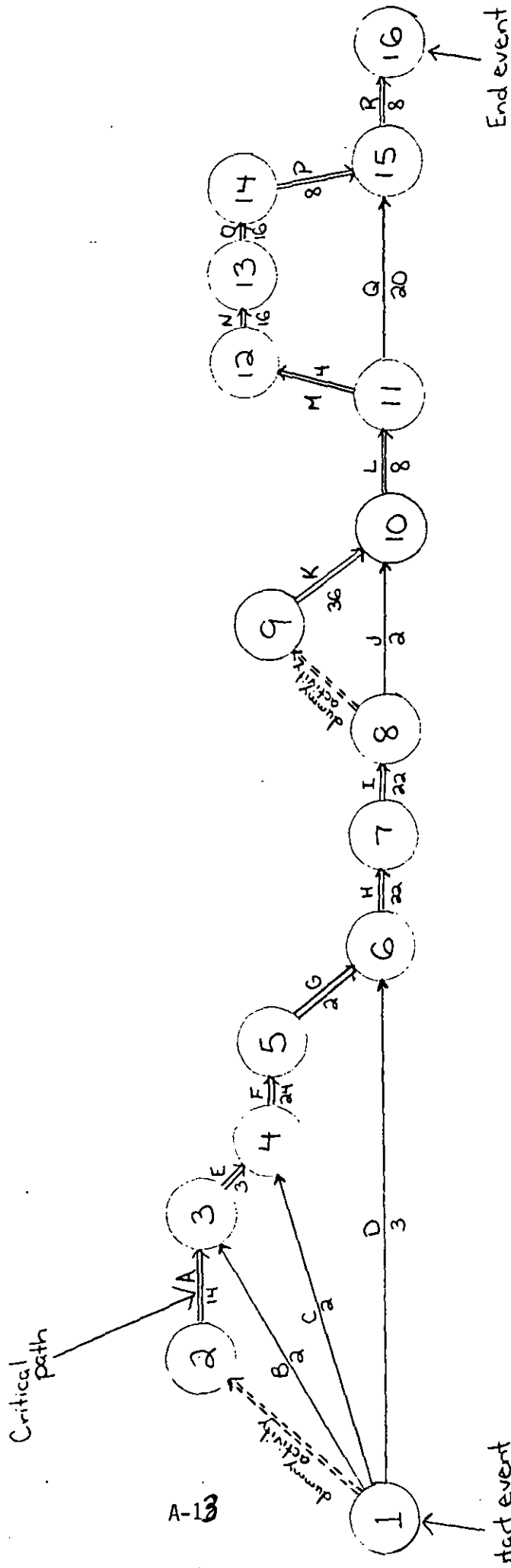
Activity Code Name	Predecessor Activity	Duration (hrs)
A	-----	14
B	-----	2
C	-----	2
D	-----	3
E	A, B	3
F	C, E	24
G	F	2
H	D, G	22
I	H	22
J	I	2
K	I	36
L	J, K	8
M	L	4
N	M	16
O	N	16
P	O	8
Q	L	20
R	P, Q	8

CRITICAL PATH ANALYSIS

Successor Event	Predecessor Event	te (hrs)	Te (hrs)	Tl (hrs)	Slack (hrs)
(END) 16	15	8	183	183	0
15	14	8	175	175	0
15	11	20	151	175	24
14	13	16	167	167	0
13	12	16	151	151	0
12	11	4	135	135	0
11	10	8	131	131	0
10	9	36	123	123	0
10	8	2	89	123	34
9	8	0	87	87	0
8	7	22	87	87	0
7	6	22	65	65	0
6	5	2	43	43	0
6	1	3	3	43	40
5	4	24	41	41	0
4	3	3	17	17	0
4	1	2	2	17	15
3	2	14	14	14	0
3	1	2	2	14	12
2	1 (START)	0	0	0	0

*Every event is on the critical path

PERT/CPM NETWORK



Critical Path: 1-2-3-4-5-6-7-8-9-10-11-12-13-14-15-16

* Denoted on network by double arrow, \Rightarrow

INTRODUCTION

The objective of this project was to design a bridge according to the standards for durability, constructability, usability, strength and serviceability. This design has been carried out in accordance with the rules provided by the American Institute of Steel Construction.

PROJECT DESCRIPTION

The members and connections of the bridge have been designed for strength and ease in assembly according to the AISC guidelines. The fabrication and materials have been studied to ensure the most economical process.

EQUIPMENT LIST

All of the needed equipment is available in the SIUC workshop located on the ground floor of Engineering Building D. The equipment in the workshop is as follows:

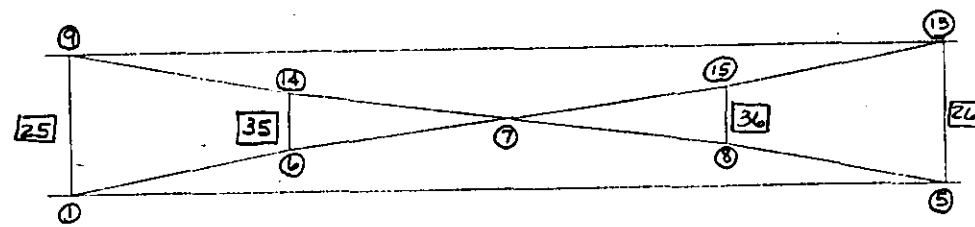
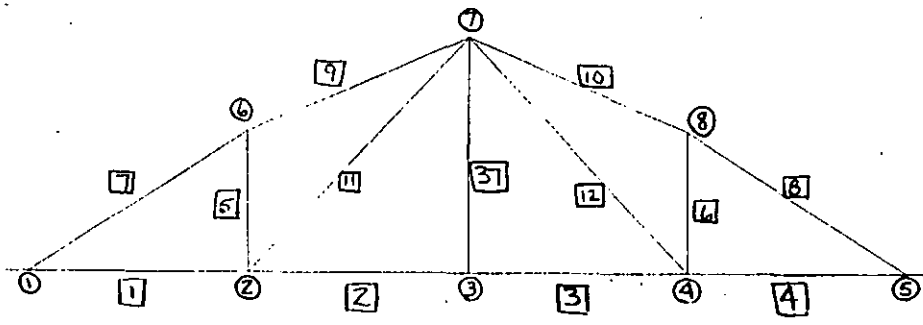
- 1) Delta Milwaukee drill press
Model # MD 6X110 CW (1/3 hp)
- 2) Emerson 7" horizontal metal cutting band saw
Model # 10-1720T
- 3) Enco vertical band saw
Model # 165-1551
- 4) Tri-star 6" electric bench grinder
- 5) Arc welder
- 6) Power hand drill
- 7) Assorted hand files
- 8) Safety glasses

Note: John Hester is in charge of the workshop and permission must be obtained from him before any work begins. Also, identification cards must be obtained for those students who will be working on the bridge in the workshop during the weekends.

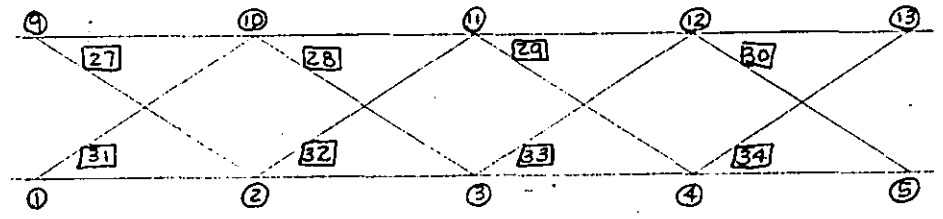
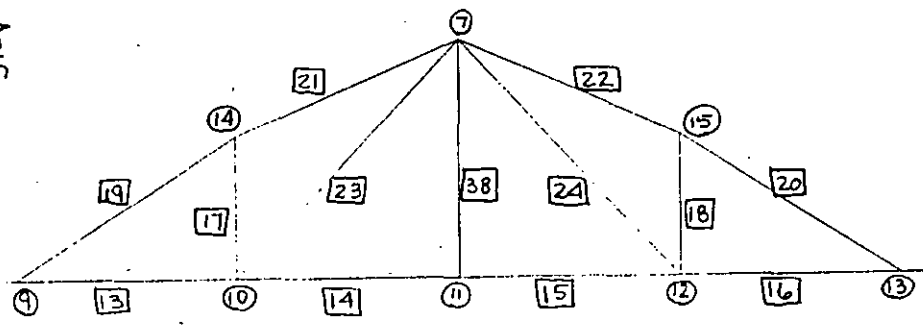
MATERIALS LIST

ITEM	DIMENSIONS	QTY	LINEAR INCHES*	DESIRED STRENGTH
Structural Steel Tubing (Members 25, 26)	1/2" x 1/2" x 0.049"	2	36.0	Fy = 36 ksi
Structural Steel Tubing (Members 35, 36)	1/2" x 1/2" x 0.049"	2	14.4	Fy = 36 ksi
Structural Steel Tubing (Members 27-34)	5/8" x 5/8" x 0.049"	8	64.9	Fy = 36 ksi
Structural Steel Tubing (Members 7, 8, 19, 20)	1" x 1" x 0.049"	4	65.8	Fy = 36 ksi
Structural Steel Tubing (Members 9, 10, 21, 22)	1" x 1" x 0.049"	4	59.5	Fy = 36 ksi
Structural Steel Tubing (Members 1, 4, 13, 16)	1 1/4" x 1 1/4" x 0.049"	4	60.0	Fy = 36 ksi
Structural Steel Tubing (Members 2, 3, 14, 15)	1 1/4" x 1 1/4" x 0.049"	4	54.0	Fy = 36 ksi
Structural Steel Tubing (Connections)	1 1/4" x 1 1/4" x 0.083"	1	72.0	Fy = 36 ksi
Structural Steel Tubing (Connections)	1 1/2" x 1 1/2" x 0.109"	1	24.0	Fy = 36 ksi
Round Threaded Steel Rods (Members 5, 6, 17, 18)	1/4" diam	4	36.0	Fy = 36 ksi
Round Threaded Steel Rods (Members 11, 12, 23, 24)	1/4" diam	4	82.4	Fy = 36 ksi
Round Threaded Steel Rods (Members 37, 38)	3/8" diam	2	60.0	Fy = 36 ksi
Steel Turnbuckles	1/4" threading	4	-----	325 lb (T)
Steel Turnbuckles	1/4" threading	4	-----	225 lb (T)
Steel Turnbuckles	3/8" threading	2	-----	1000 lb (T)
Angle	1" x 1" x 1/8"	1	60.0	-----
Dent Ring Pins	1/4" x 1 3/4"	40	-----	-----
Elevator Bolts	1/4" x 2"	20	-----	-----
Eye Bolts	3/8" x 1 1/4"	9	-----	1400 lb
Loose hinges	1"	8	-----	-----
Containers of Acetone	1 pint	2	-----	-----
X-O Rust Primer	1 pint	2	-----	-----
Spray Paint (Enamel)	12 ounces	4	-----	-----
WD-40 Lubricant	6 ounces	2	-----	-----

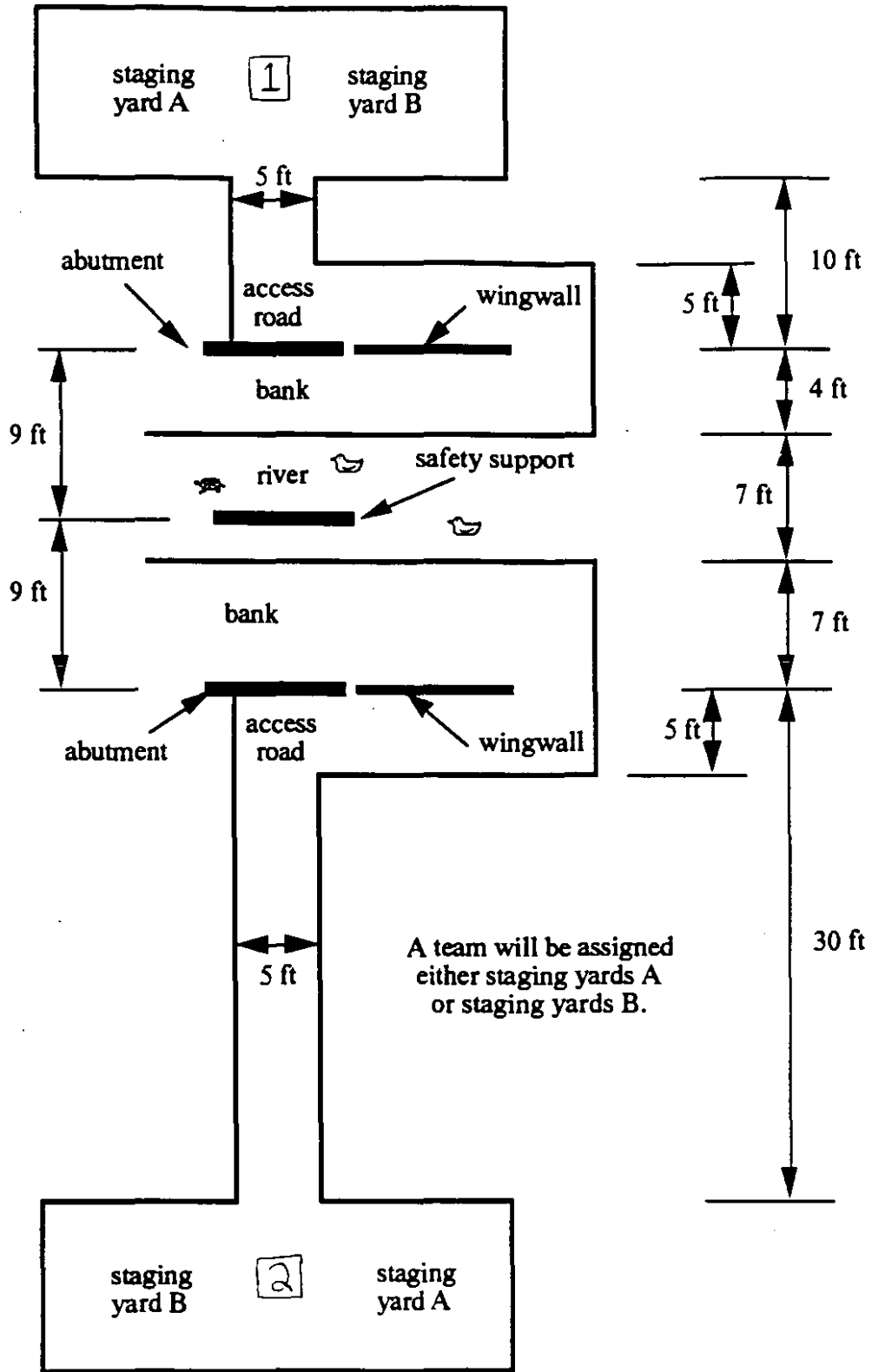
*These are the exact member lengths. When ordering when cutting the steel, some extra length should be added. It is easy to cut off extra but nearly impossible to lengthen a member which is too short.



A-16



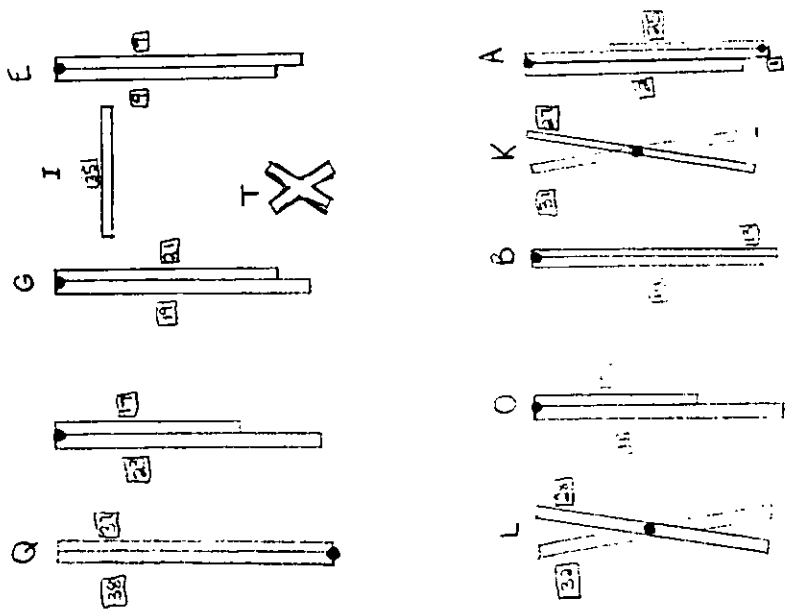
3	4/07	RLD	Modified Members
2	3/22	RLD	Changed Height
1	3/08	RLD	Original
Rev	Date	By	Purpose
SALUKI ENGINEERING COMPANY			
Team #6		SEC Reference #DES.06.S95	
Client: Egyptian Associates		EA Reference #: BRIDGE06.S95	
Title: Member and Joint Numbers			
Drawn by: Rachel Davis		Scale: 1"=2'	
Date: 4/24/95	Drawing Number: 001	Rev:	3



Site Plan

COMPETITION STAGING YARD SET-UP

STAGING YARD 1 (SHORT IDE)



← Assuming Staging Yard "A" will be used

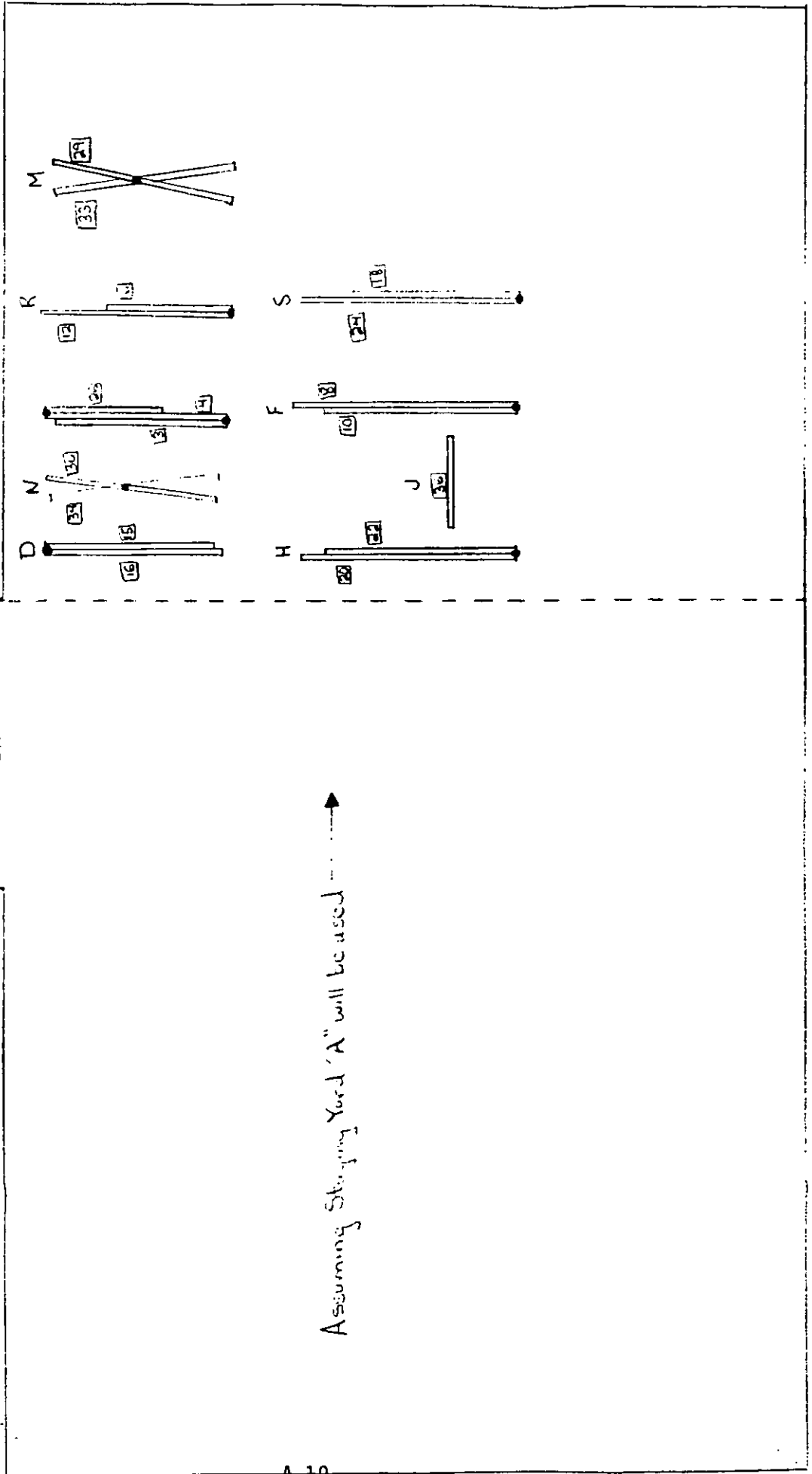
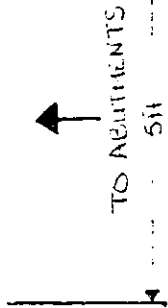
5ft
TO ADJUTMENTS

• denotes hinge at this point

*Not to scale, staging yard size subject to vary
This drawing is intended to show only the relative positions of the members

COMPETITION STAGING YARD SETUP

STAGING YARD 2 (LONG SLIDE)



Assuming Staging Yard 'A' will be used

* Not to scale. Staging yard 'A' will be used for every...
 • denotes length of this point.

BASIS OF DESIGN

The following documents and standards have served as the basis for the Saluki Engineering Company eleven week design study of the AISC steel bridge:

Documents:

- | | |
|---|-------------------|
| I. Request for Proposal
from Egyptian Associates | January 31, 1995 |
| A. Project Definition | January 31, 1995 |
| B. Additional Requirements | January 31, 1995 |
| II. Saluki Engineering Proposal | February 13, 1995 |
| III. Transmittal Letter | February 13, 1995 |
| IV. Saluki Engineering Progress Report | March 21, 1995 |

Standards:

- | | |
|--|------------------|
| I. Saluki Engineering Company Standards | January 17, 1995 |
| II. American Institute of Steel Construction Standards | 1986 |

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103 Top Chord 7,8,19,20	B-11
104 Top Chord 9,10,21,22	B-12
VII. Bibliography	B-13

INTRODUCTION

The design of the steel members of the bridge is a process of compromise. In competition, the major categories in determining which bridge wins overall, are the weight of the bridge, the deflection of the bridge, and the speed of construction of the bridge. While the speed of construction is mostly a result of the connection design, the weight of the bridge and the deflection of the bridge are very much dependent upon the member design.

The compromise lies in the sizing of the members. Of course the deflection of the bridge could be minimized by the use of over-sized, over-designed members, however, the bridge will suffer in the category of weight. At the other extreme, very small members could be used in order to minimize the weight of the bridge, however, the bridge will suffer in the category of deflection and may possibly even fail. An efficient design of the members must be pursued so that the bridge will perform well in both the categories of weight and deflection.

TECHNICAL DISCUSSION

The members of the bridge are to be a combination of square tubing and threaded rods. In all there will be four different cross-sections of square tubing used and two different diameters of threaded rods.

BOTTOM CHORD MEMBERS

The bottom chord members will be 1 1/4 inch square tubing with a wall thickness of 0.049 inches. These members are detailed in drawings 101 and 102 of this section.

In the design of the bottom chord, which is subjected to a combination of bending and tensile forces, both I-beams and square tubing were investigated. I-beams, although very strong in bending, lack resistance to torsion due to their open faces. In addition, it was discovered that the acquisition of I-beams small enough for the bridge would be very difficult and most likely prohibitively expensive. The investigation of square tubing yielded more promising results. Square tubing has considerable strength in bending, although less than I-beams for the same area. However, square tubing has the advantage of significant torsional strength due to the closed faces of the cross-section. And, perhaps more important, square tubing is readily available in sizes all the way down to 1/2 inch square, which would allow the freedom to design for the most efficient members possible. For these reasons, square tubing was selected for the bottom chord members.

TOP CHORD MEMBERS

The top chord members will be 1 inch square tubing with a wall thickness of 0.049 inches. These members are detailed in drawings 103 and 104 of this section.

TOP CHORD MEMBERS CONT. . .

In the design of the top chord, which will be subjected to compressive forces, square tubing was selected from the beginning. The selection was motivated by the efficiency of square tubing when subjected to compression. The only more efficient member type under compression is circular tubing, but circular tubing complicated the connections of the bridge. The efficiency of square tubing is a result of the nearly equal radius of gyration in all directions which provides for a nearly equal resistance to buckling in all directions. The member is only as strong as its weakest axis and so members which are unsymmetrical contain wasted material in their strong axis.

The aim in designing the cross-section was to have the mass as far away from the axial center of the tube as possible. This is because the radius of gyration and hence buckling resistance for a given cross-sectional area increases as the moment of inertia of the cross-section increases. So, whereas 3/4 inch square tubing could have been selected to resist the compressive load, the members would have been much thicker and therefore much heavier than the 1 inch square members which were selected.

LATERAL BRACING MEMBERS

The diagonal lateral bracing members will be 5/8 inch square tubing with a wall thickness of 0.049 inches. The remaining lateral bracing will be 1/2 inch square tubing.

The forces in the lateral bracings are relatively small, with no member being subjected to an axial force of even 200 lbs. However, the force in any given lateral bracing may be either tension or compression depending upon which side the 100 lb lateral test load. The compression state will dominate and so all of the members were designed for the compression loading and hence, square tubing was employed for the same reasons outlined in the "Top Chord Members" explanation above.

*See Section D for drawings and additional specifications on lateral bracing.

WEB MEMBERS

The web members will be 1/4 inch diameter threaded rods and 3/8 inch diameter threaded rods.

In order to significantly reduce the overall weight of the bridge, a truss pattern in which all of the web members are in tension was carefully chosen. Since tensile forces tend to straighten the member, buckling is not a concern and thus the members can be made very small and light.

To carry the tensile force in the web members we had the option of using cables or rods. The concern with cables was excessive stretching, and since deflection is a major concern in the competitiveness of the bridge, we ruled out the use of cables. Instead, we sacrificed some lightness in the bridge in order to gain considerable stiffness with the use of rods. Threaded rods were called for so that turnbuckles could be incorporated at one of the connections of each rod. This will ensure the tight fit of the rods and the rigidity of the bridge as a whole.

*See Section D for drawings and additional specifications on web members.

FINAL ANALYSIS OF BRIDGE FOR FORCES AND DEFLECTIONS

The final analysis of the bridge for the forces and deflections was performed by computer.

Dr. Aslam Kassimali's structural analysis computer program was used in order to determine the forces in each member of the bridge when the bridge was either subjected to the 2500 lb vertical loading test or the 100 lb lateral loading test. The bridge was analyzed as a truss, which includes the assumptions that all of the loading occurs at the joints and that the axial centroid of the members meet at a single point at the joints. In order to accommodate the assumption of loading only at the joints, the distributed loading of 2500 lb along with an assumed bridge weight of 150

FORCES AND DEFLECTIONS CONT...

lb was applied as a downward 662.5 lb loading at each of joints 3 and 11, and a downward 331.3 lb loading at each of joints 2, 4, 10, and 12. As for the 100 lb lateral loading test, no modeling was needed since it is actually applied as a point load at the joint during competition.

There were difficulties in using the structural analysis computer program in order to analyze for the deflections in the bridge as a result of these two loading tests. These difficulties lay in the fact that our bridge contains members of 6 different cross-sections and the program would only accept four different cross-sections. As a result the method of virtual work was employed along with the assistance of a spreadsheet. This method revealed a vertical deflection of 0.109 in at the center of the bridge due to the 2500 lb vertical load test, and a lateral deflection of 0.019 in at the center of the bridge due to the 100 lb lateral load test. These are very promising results and bodes well for the competitiveness of the bridge.

*See the appendices of this report for the detailed results of the computer analysis and the virtual work method.

MEMBER MATERIALS LIST

ITEM	DIMENSIONS	QTY	LINEAR INCHES*	DESIRED STRENGTH
Structural Steel Tubing (Members 7, 8, 19, 20)	1" x 1" x 0.049"	4	65.8	Fy = 36 ksi
Structural Steel Tubing (Members 9, 10, 21, 22)	1" x 1" x 0.049"	4	59.5	Fy = 36 ksi
Structural Steel Tubing (Members 1, 4, 13, 16)	1 1/4" x 1 1/4" x 0.049"	4	60.0	Fy = 36 ksi
Structural Steel Tubing (Members 2, 3, 14, 15)	1 1/4" x 1 1/4" x 0.049"	4	54.0	Fy = 36 ksi

*These are the exact member lengths. When ordering and cutting the steel, some extra length should be added. It is easy to cut off extra but nearly impossible to lengthen a member which is too short.

COSTING SUMMARY

Materials:

Structural Steel Tubing:

Type	Length	Quantity	Cost/each	Vendor
1" x 1" x 0.049"	6'	8	\$10.69	TVH
1 1/4" x 1 1/4" x 0.049	6'	8	\$12.59	TVH

Vendors:

TVH = True Value Hardware

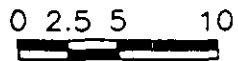
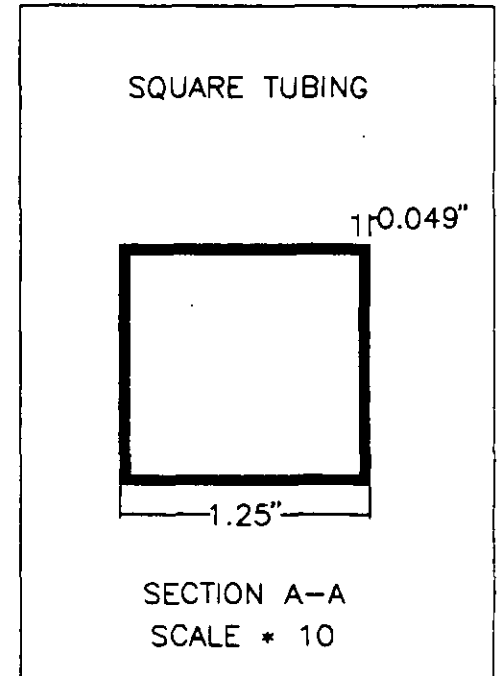
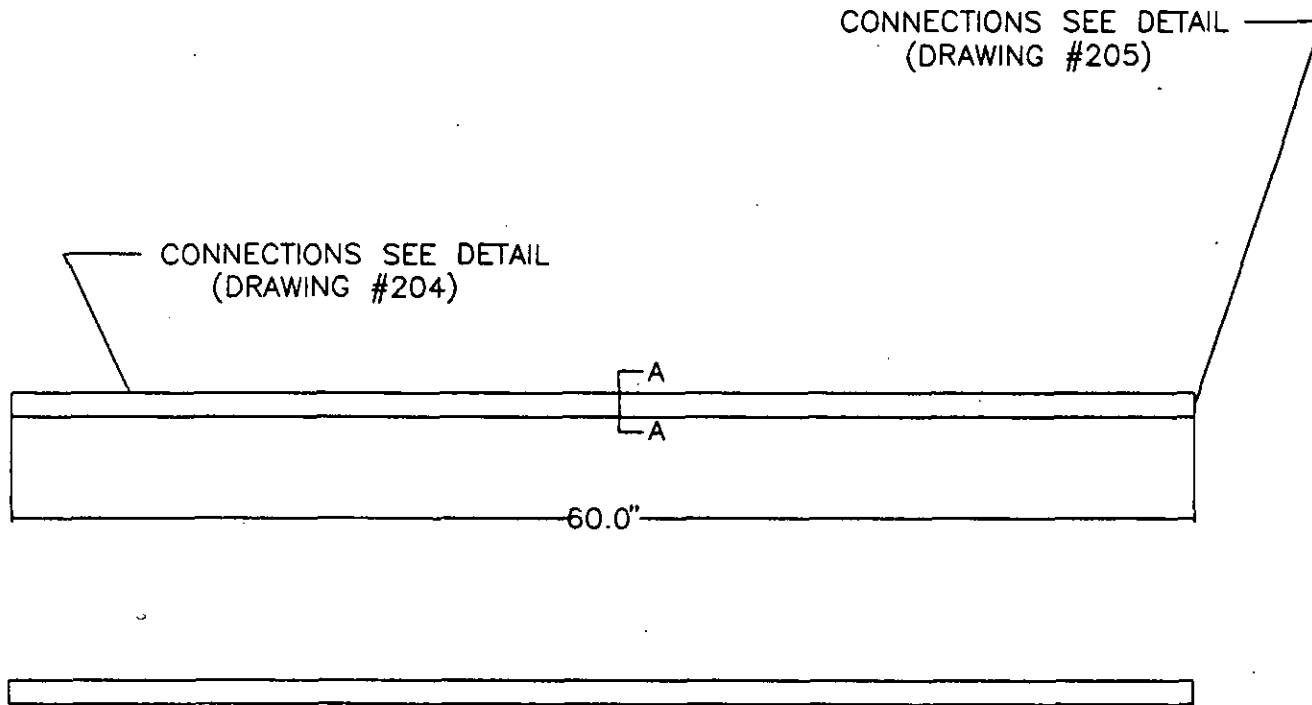
M-C = McMaster - Carr Supply Company

Labor and Equipment:

*Since all sections are interdependent this is covered in the Team Section only.

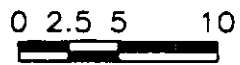
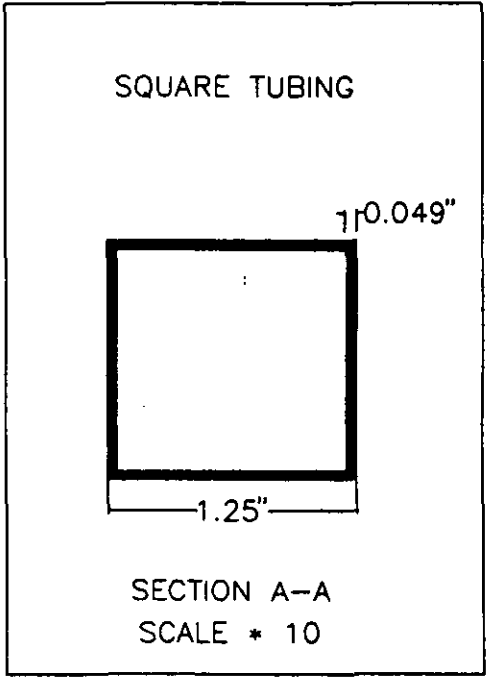
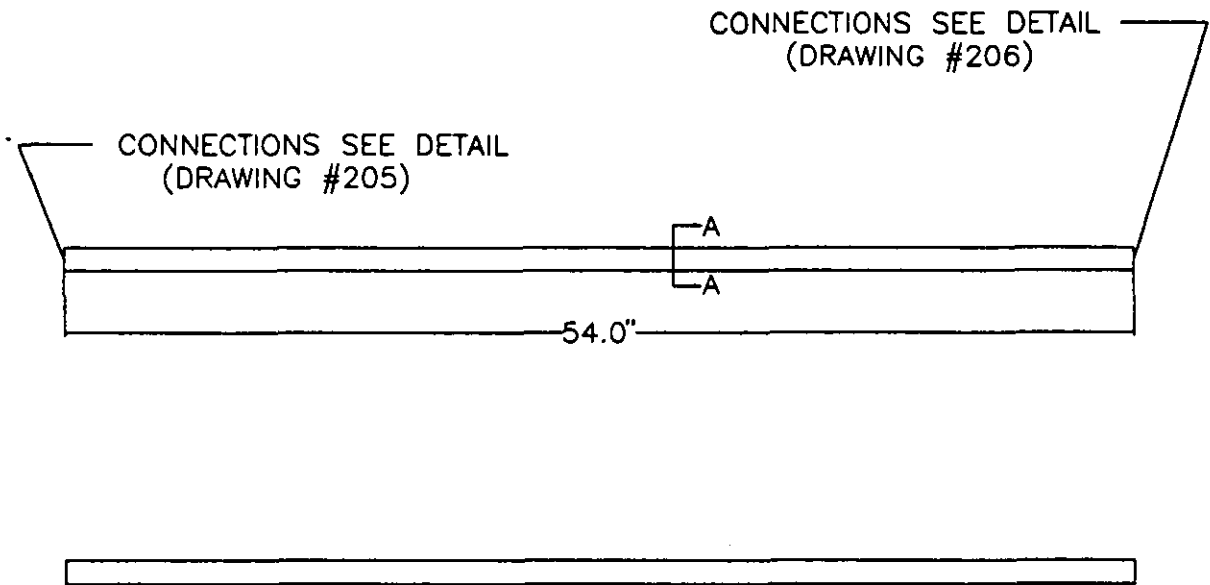
Total Materials Cost = \$186.24

B-9

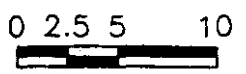
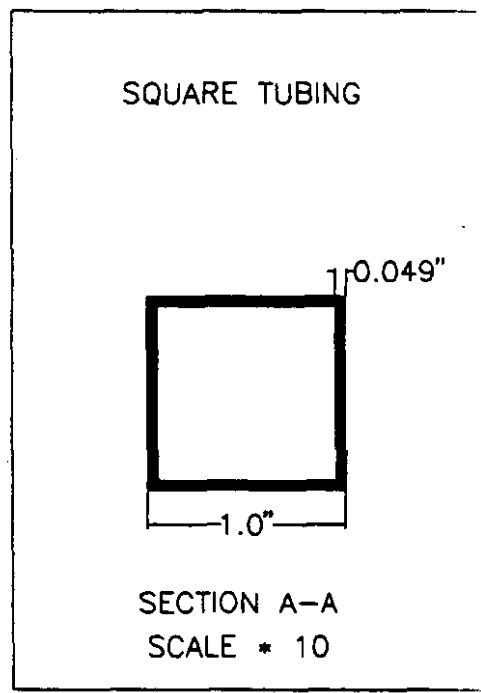
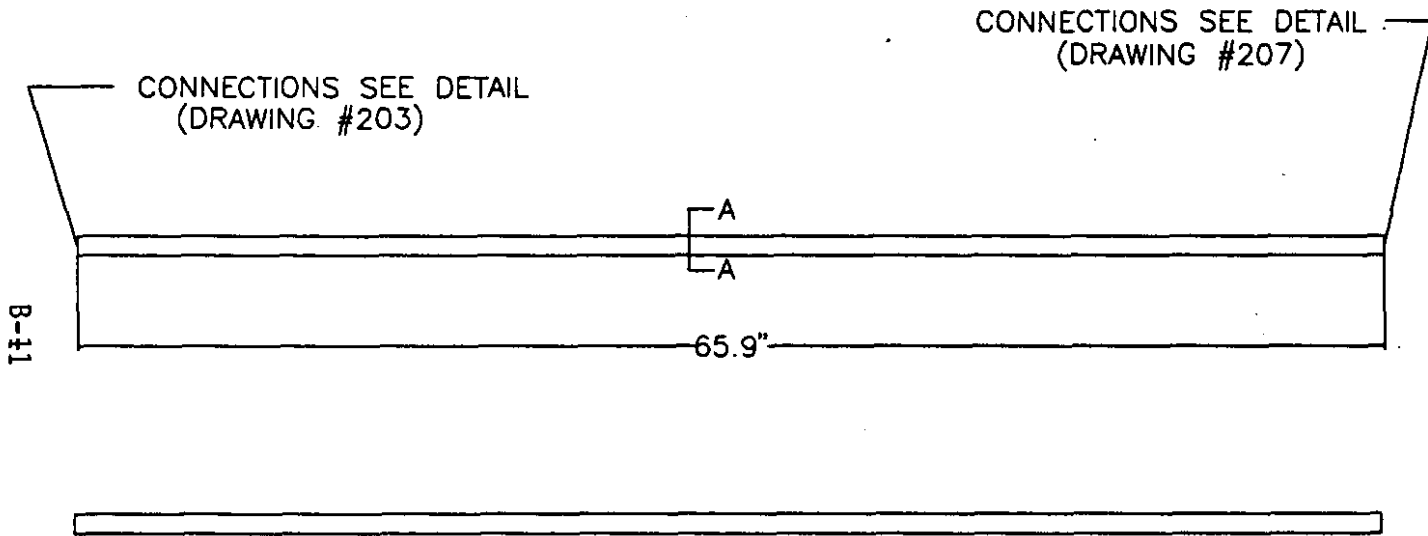


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Rev	Date	By	Purpose
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Team #6		SEC Reference #DES.06.S95	
Client:		EA Reference #:	
Egyptian Associates		BRIDGE06.S95	
Title: BOTTOM CHORD			
MEMBERS 1, 4, 13, 16			
Drawn by: DEREK PEEBLES			Scale: 1:1
Date:		Drawing Number:	
4/17/95		101	
			Rev #
			0

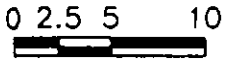
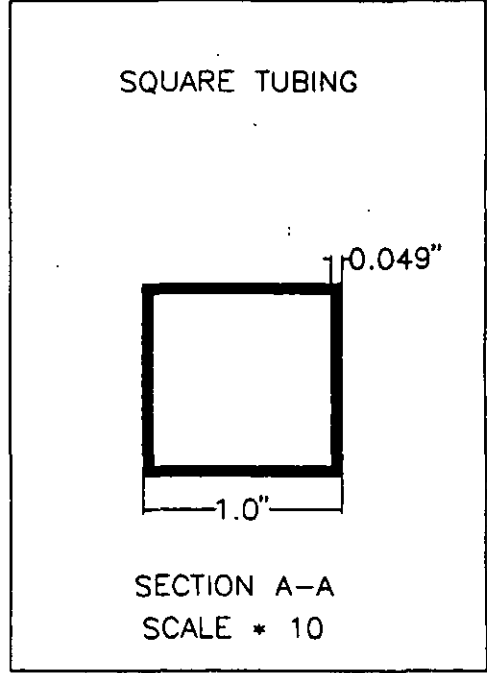
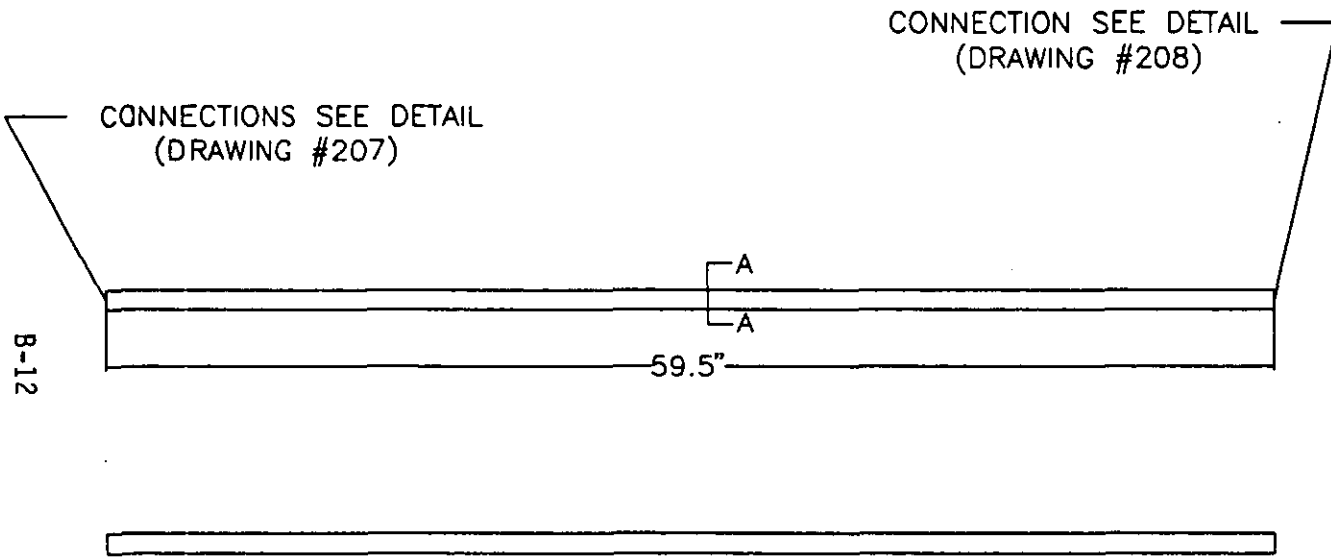
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Rev	Date	By	Purpose
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Team #6		SEC Reference #DES.06.S95	
Client:		EA Reference #:	
Egyptian Associates		BRIDGE06.S95	
Title: BOTTOM CHORD			
MEMBERS 2, 3, 14, 15			
Drawn by: DEREK PEEBLES		Scale: 1:10	
Date:	Drawing Number:		Rev.
4/17/95	102		0



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Rev	Date	By	Purpose
SALUKI ENGINEERING COMPANY			
Team #6		SEC Reference #DES.06.S95	
Client:		EA Reference #:	
Egyptian Associates		BRIDGE06.S95	
Title: TOP CHORD			
MEMBERS 7, 8, 19, 20			
Drawn by: DEREK PEEBLES		Scale: 1:10	
Date:	Drawing Number:	Rev.	
4/17/95	103	0	



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Rev	Date	By	Purpose
SALUKI ENGINEERING COMPANY			
Team #6		SEC Reference #DES.06.S95	
Client: Egyptian Associates		EA Reference #: BRIDGE06.S95	
Title: TOP CHORD MEMBERS 9, 10, 21, 22			
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Date: 4/17/05	Drawing Number: 104		Rev. "

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SECTION C

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IV. Assembly Process	C-6, C-7		
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VII. Drawings			
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202	Member and Joint Numbers	all	C-11
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204	Bottom End Connections	1, 5, 9, 13	C-13
205	Bottom Inner Connections	2, 4, 10, 12	C-14
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INTRODUCTION

This section contains the design of the bridge member connections as well as the assembly process of the final bridge for the AISC Bridge-Building Competition. The design of the connections is important in order to limit the deflection of the assembled bridge and to make the assembly time a minimum. The compression connections will be steel tube sleeves to hold the member in place. The tension connections will be connected with hooks and eyes. Other connections, such as those with little load, torsional loads, or alternating loads will be pinned or welded.

The assembly process is important in the design of the entire bridge. AISC rules limit the size and weight of the members, the time of assembly, and the number of preassembled members. The recommended assembly process will use four team members to assemble the bridge in approximately three minutes. It will also give a logical order the assembly to keep organization and to maximize the use of time by each team member.

TECHNICAL DISCUSSION

Connections:

Joints 1, 5, 9, 13

These connections consist of a 7-in. section of 1-1/4" x 1-1/4" x 0.083" square tubing welded to the top of the end bottom chord member at the angle of the upper chord member. The inside face of the sleeve will be removed to allow the member to slide in easily. There will be a 3-in. section of 1" x 1" x 1/8" angle welded to the inside of the end bottom chord member. The end lateral member will be pinned to the angle so that it will be able to fold into the angle. This member will be connected to the angle at one joint and pinned during assembly to the angle at the opposite joint. There will also be a hole for the crossed lateral member to be attached with an elevator bolt. (See Drawing #202 for locations and Drawing #204 for details.)

Joints 2, 4, 10, 12

These connections consist of two bottom chord members hinged at the bottom of the members with a 1-in. hinge. A 6-in. section of 1" x 1" x 1/8" angle will be welded to the inside of the bottom chord member. There will be two holes to pin the members in place to the angle when unfolded. There will also be two holes for the crossed lateral members to be connected. A hook, taken from the turnbuckle, will be welded to the bottom chord member to attach the rings to the rods. (See Drawing #202 for locations and Drawing #205 for details.)

Joints 3, 11

These connections consist of an 8-in. section of 1-1/2" x 1-1/2" x 0.109" square tubing welded to one of the center bottom chord members. There will be a 6-in. section of 1" x 1" x 1/8" angle welded to the inside of the tubing. There will be holes for pinning the bottom chord members in place inside the sleeve and for the crossed lateral members to be connected. There will also be a hook, taken from the turnbuckle, to connect the rings welded to the rods. (See Drawing #202 for locations and Drawing #206 for details.)

Joints 6, 8, 14, 15

These connections will consist of two sleeves of 1-1/4" x 1-1/4" x 0.083" square tubing welded at the angle of the top chord members. The bottom of the sleeves will be open in order to place onto the upper chord members. The sleeves will be welded to the upper lateral member. The two upper chord members will be hinged to allow folding before the competition. There will be two holes for pins in each sleeve and a hook, taken from the turnbuckle, welded to the inside of the sleeves. (See Drawing #202 for locations and Drawing #207 for Details.)

Joint 7

This connection will consist of four 1-1/4" x 1-1/4" x 0.083" square tubing sleeves welded together at the angles of the top chord members. A hook, taken from the turnbuckle, will be welded underneath. There will be two holes in each sleeve to hold the upper chord members in place. (See Drawing #202 for locations and Drawing #208 for Details.)

Saluki Engineering Company
Final Report for Egyptian Associates
Project No: BRIDGE06.S95
SEC No: DES06.S95

April 26, 1995
Revision 0

Due to the length of members 11, 12, 23, and 24, two rings must be welded to the rods at the mid-section to create a hinge, which will keep the length of the member under the specified 66 inches.

The assembly process has been designed for a four-person team. This seemed to work the best in the last four competitions. The bridge should be able to be assembled in about three minutes, which would result in a winning construction speed score in the last four competitions. For more details on the assembly process, see pages C-6 and C-7.

ASSEMBLY PROCESS

Preassembled Members*:

1, 2, 25

13, 14

3, 4, 26

15, 16

7, 9

8, 10

19, 21

20, 22

35

36

27, 31

28, 32

29, 33

30, 34

5, 11

17, 23

37, 38

6, 12

18, 24

Connection Sleeve (Joint #7)

Assembly Letter:

A

B

C

D

E

F

G

H

I

J

K

L

M

N

O

P

Q

R

S

T

*Refer to Drawing #202 for location of
members and joints

ASSEMBLY PROCESS (Continued)

Staging Yard (Short Side):

Team Members: TM1, TM2

Assembly Members:

A, B, E, G, I, K, L, O, P, Q, T

Staging Yard (Long Side):

Team Members: TM3, TM4

Assembly Members:

C, D, F, H, J, M, N, R, S

TIMED ASSEMBLY PROCEDURE:

TM1 and TM2 unfold A, B, K, connect and carry to abutments

TM1 connects B, D at joint #11

TM2 carries E, G, I, T to abutments

TM1 and TM2 unfold E, G, connect E, G, I, T, and slip into sleeves at joints #9, #10
(do not pin bottom chord)

TM1 carries O, then Q, then L to abutments

TM2 carries P, connects P, O

TM1 and TM2 connect Q, L

TM1 and TM2 connect rods to bottom chord
(slip E, G out of bottom sleeve to hook bottom connections, then replace and pin)

TM1 and TM2 make any needed adjustments and return to staging yard

TM3 and TM4 unfold C, D, N, connect and carry to abutments

TM3 connects A, C at joint #3

TM4 carries F, H, J to abutments

TM3 and TM4 unfold F, H, connect F, H, J assembly to T, slip into sleeves at joints #5, #13 (do not pin to bottom chord)

TM3 carries R, then M

TM4 carries S, connects S, R

TM3 connects M

TM3 and TM4 connect rods to bottom chord
(slip F, H out of bottom sleeve to hook bottom connections, then replace and pin)

TM3 and TM4 make any needed adjustments, then return to staging yard

CONNECTION MATERIALS LIST

ITEM	DIMENSIONS	QTY	LINEAR INCHES	DESIRED STRENGTH
Structural Steel Tubing (Connections)	1 1/4" x 1 1/4" x 0.083"	1	72.0	Fy = 36 ksi
Structural Steel Tubing (Connections)	1 1/4" x 1 1/4" x 0.109"	1	24.0	Fy = 36 ksi
Angle	1" x 1" x 1/8"	1	60.0	-----
Dent Ring Pins	1/4" x 1 3/4"	40	-----	-----
Elevator Bolts	1/4" x 2"	20	-----	-----
Eye Bolts	3/8" x 1 1/4"	9	-----	1400 lb
Loose Hinges	1"	8	-----	-----

COSTING SUMMARY

Materials:

Structural Steel Tubing:

Type	Length
1 1/4" x 1 1/4" x 0.083	6'
1 1/2" x 1 1/2" x 0.109	3'

Vendors:

TVH = True Value Hardware

M-C = McMaster Carr Supply Company

Quantity	Cost/each	Vendor
1	\$13.79	TVH
1	\$12.18	M-C

Dent Ring Pin:

Type	Quantity	Cost/each	Vendor
1/4" x 1 3/4"	40	\$2.00	TVH

Elevator Bolts:

Type	Quantity	Cost/each	Vendor
1/4" x 2"	20	\$0.32	TVH

Eye Bolts:

Type	Quantity	Cost/each	Vendor
3/8" x 1 1/4"	9	\$1.11	M-C

Angle:

Type	Quantity	Cost/each	Vendor
1" x 1" x 1/8" x 5'	1	\$22.03	M-C

Hinges:

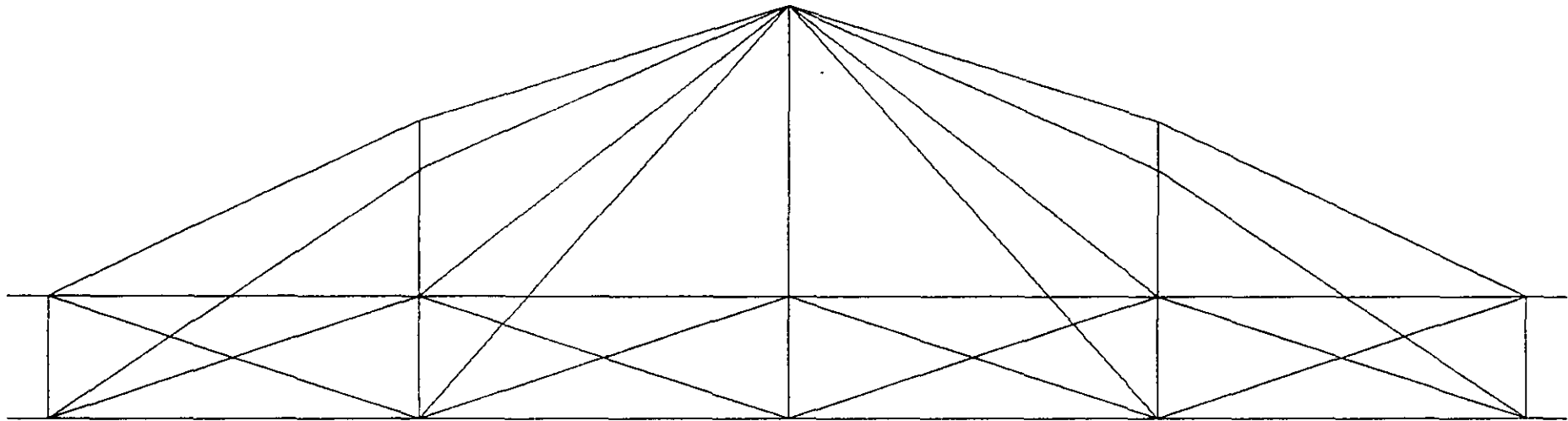
Type	Quantity	Cost/each	Vendor
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Labor and Equipment:

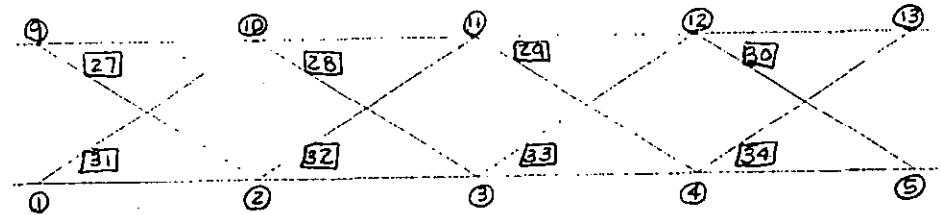
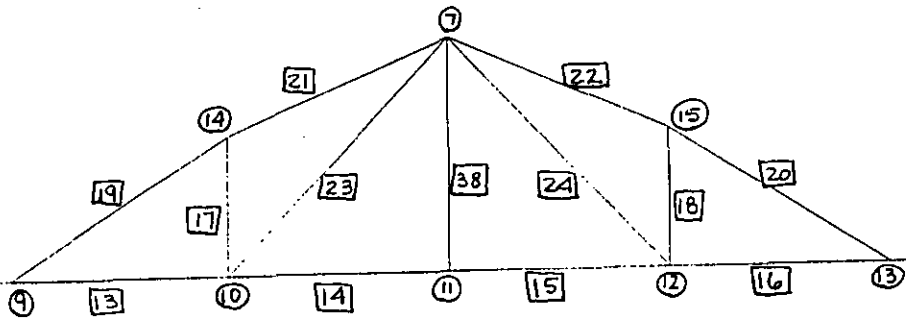
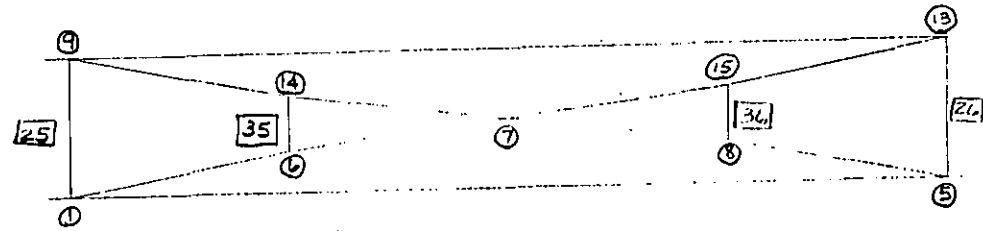
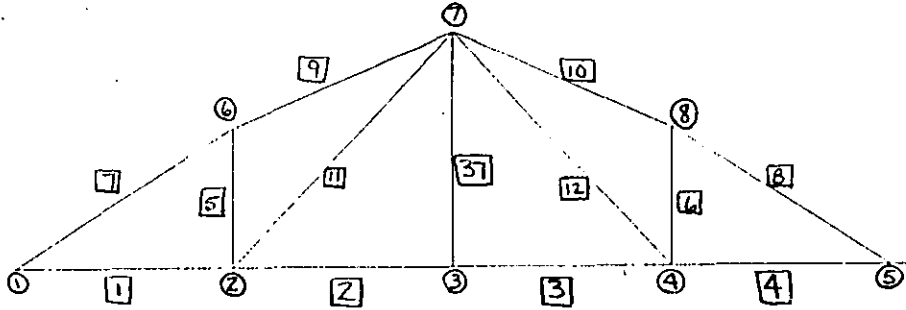
*Since all sections are interdependent this is covered in the Team Section only.

Total Materials Cost = \$154.59

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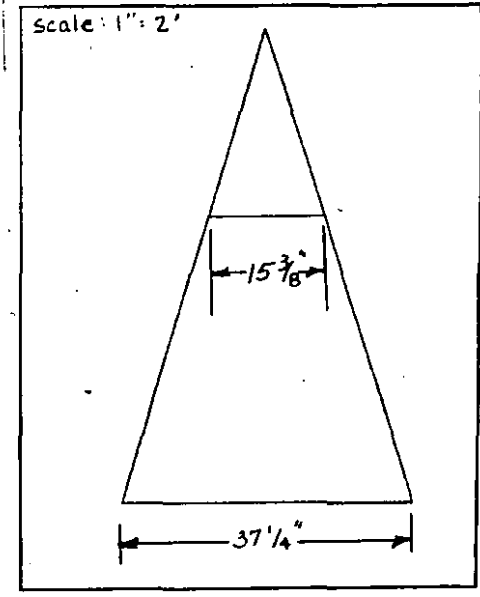
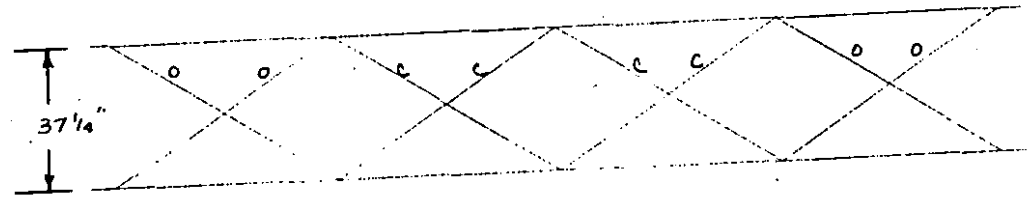
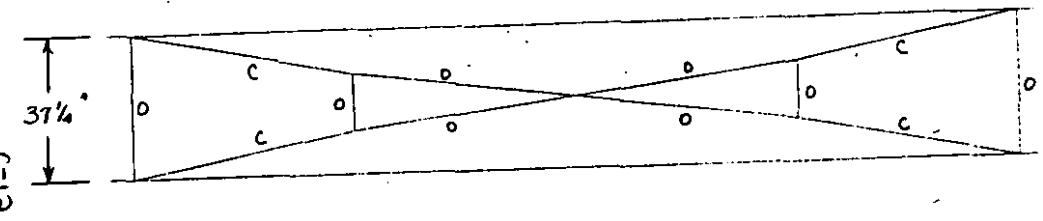
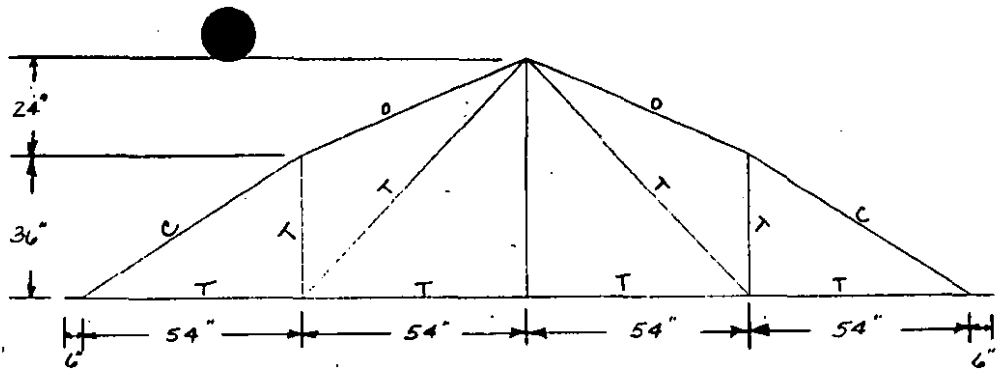


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2	3/22	RLD	Changed Height
1	3/08	RLD	Original
Rev	Date	By	Purpose
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Team #6		SEC Reference #DES.06.S95	
Client: Egyptian Associates		EA Reference #: BRIDGE06.S95	
Title: Full Bridge (3-D)			
Drawn by: Rachel Davis		Scale: 1"=2'	
Date: 4/24/95	Drawing Number: 201		Rev. 3

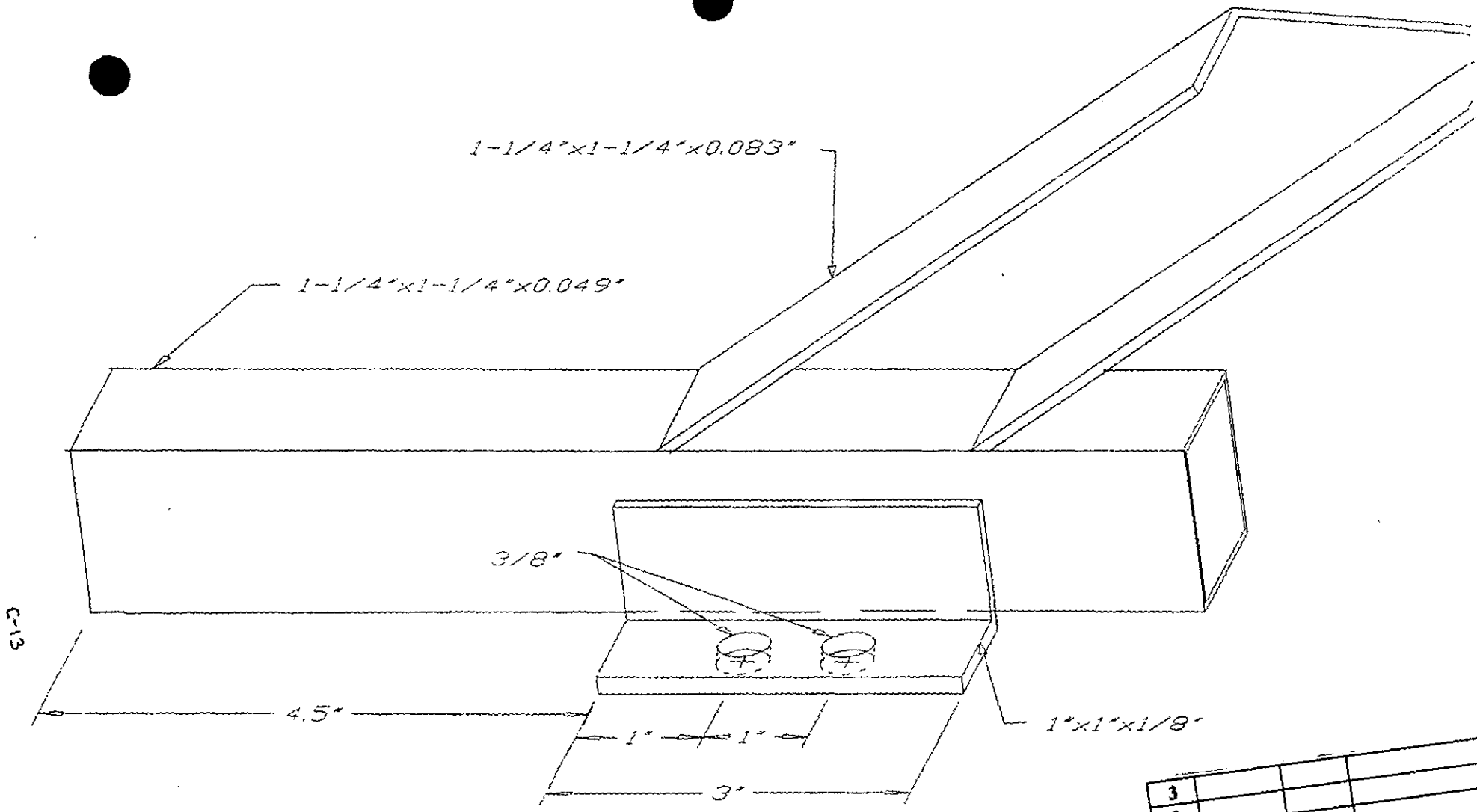


C-11

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2	3/22	RLD	Changed Height
1	3/08	RLD	Original
Rev	Date	By	Purpose
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Team #6		SEC Reference #DES.06.S95	
Client:		EA Reference #:	
Egyptian Associates		BRIDGE06.S95	
Title: Member and Joint Numbers			
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Date: 4/24/95	Drawing Number: 202		Rev. 3

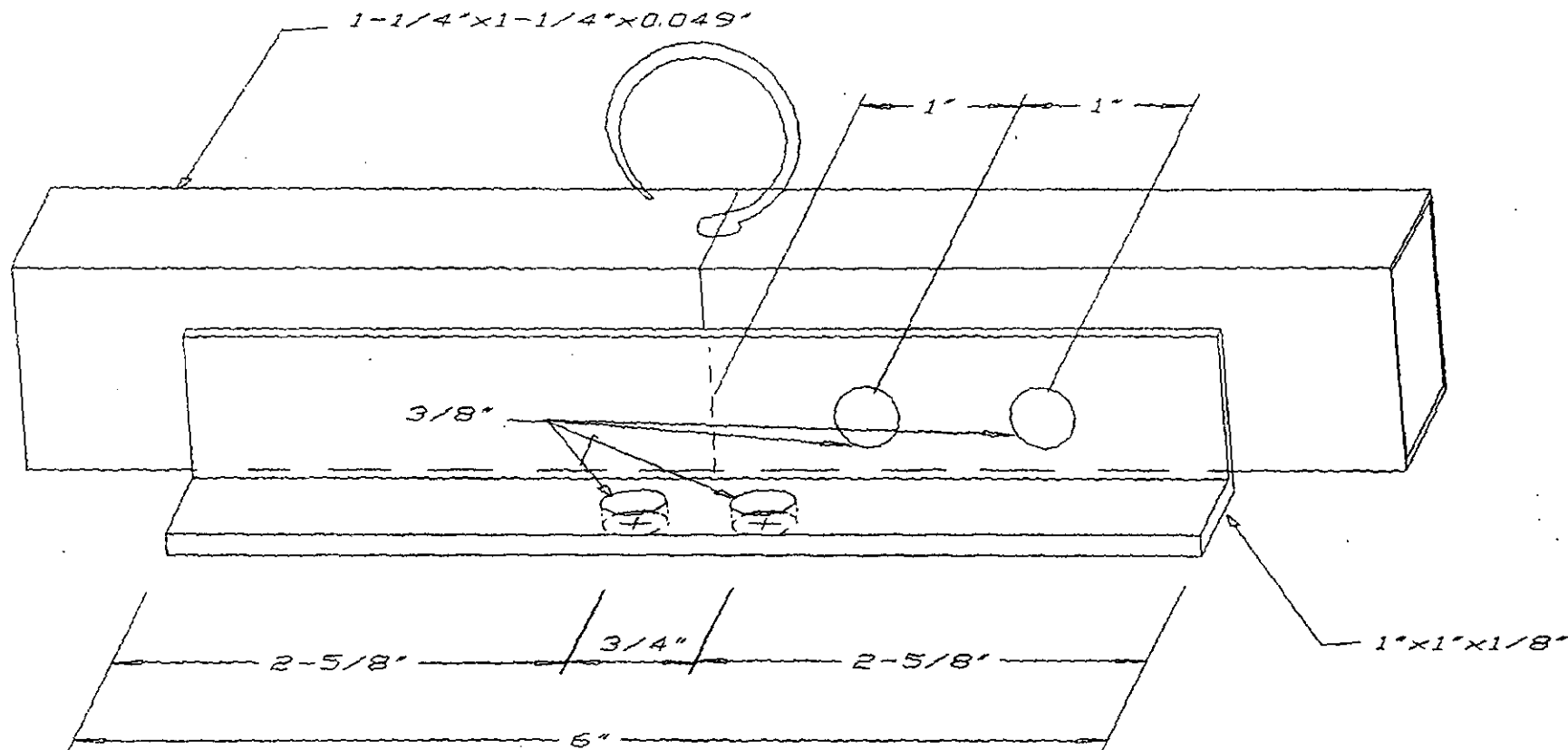


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2	3/22	RLD	Changed Height
1	3/08	RLD	Original
Rev	Date	By	Purpose
SALUKI ENGINEERING COMPANY			
Team #6		SEC Reference #DES.06.S95	
Client:		EA Reference #:	
Egyptian Associates		BRIDGE06.S95	
Title: Dimensioned Bridge			
Drawn by: Rachel Davis		Scale: 1"=2'	
Date: 4/24/95		Drawing Number: 203	
			Rev. 3



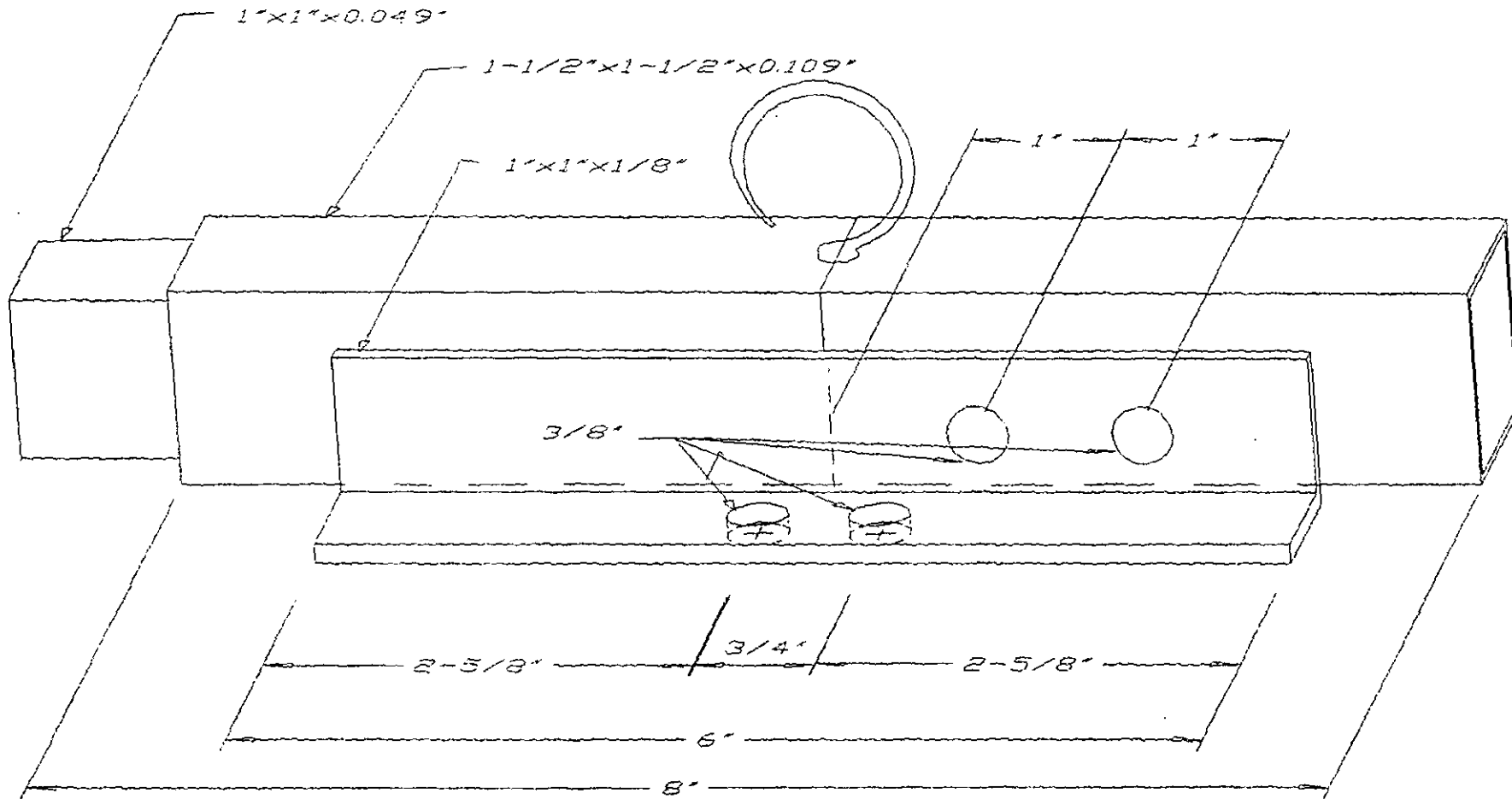
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Rev	Date	By	Purpose
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Team #6	SEC Reference #DES.06.S95		
Client:	Egyptian Associates		EA Reference #: BRIDGE06.S95
Title: Bottom End Connections (Joints #1,5,9,13)			
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Date: 4/24/95	Drawing Number:	204	Rev. 0

C-14



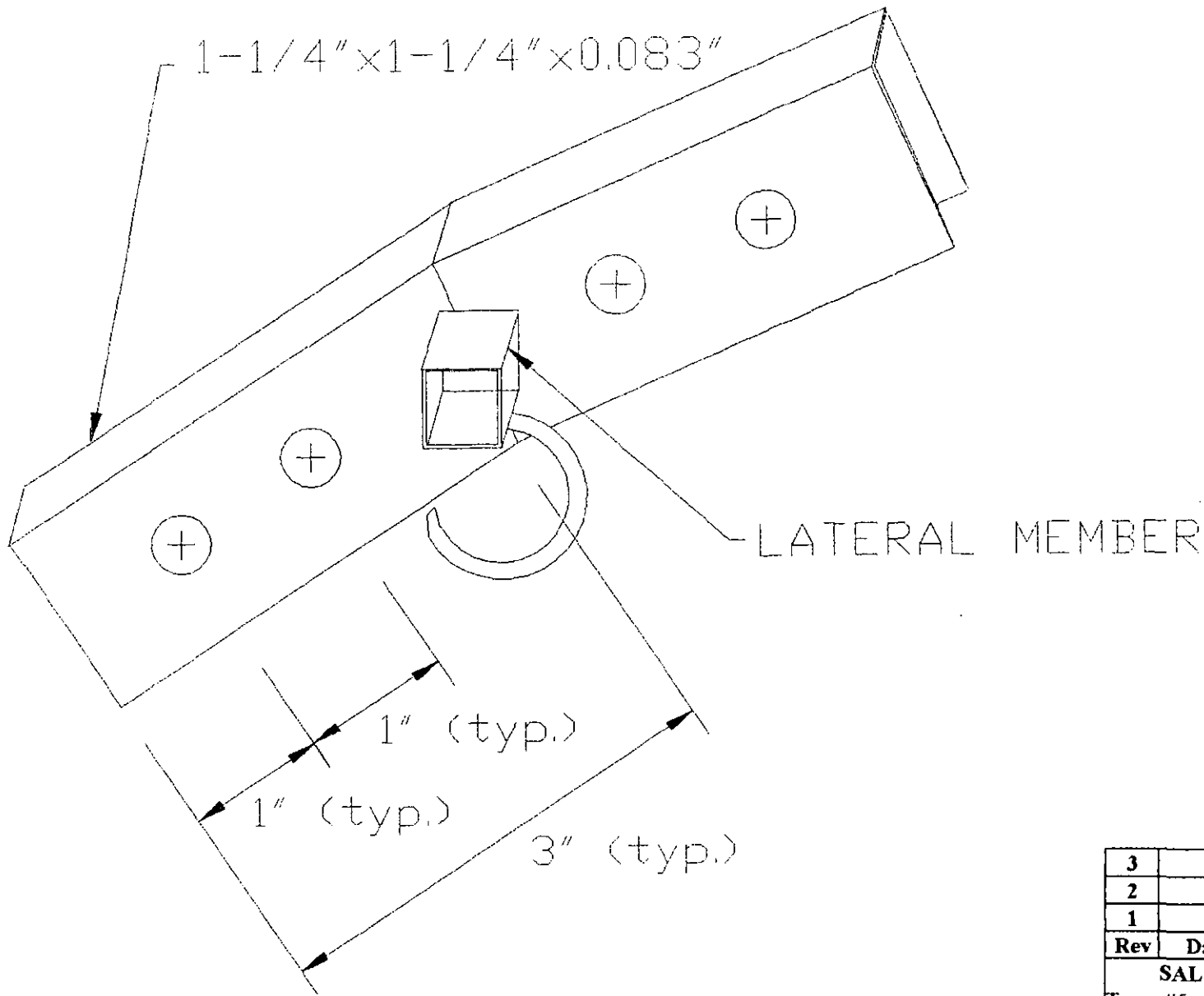
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Team #6		SEC Reference #DES.06.S95	
Client: Egyptian Associates		EA Reference #: BRIDGE06.S95	
Title: Bottom Inner Connections (Joints #2, 4, 10, 12)			
Drawn by: Rachel Davis		Scale:	1"=
Date: 4/24/95	Drawing Number: 205		Re: 0

C-15



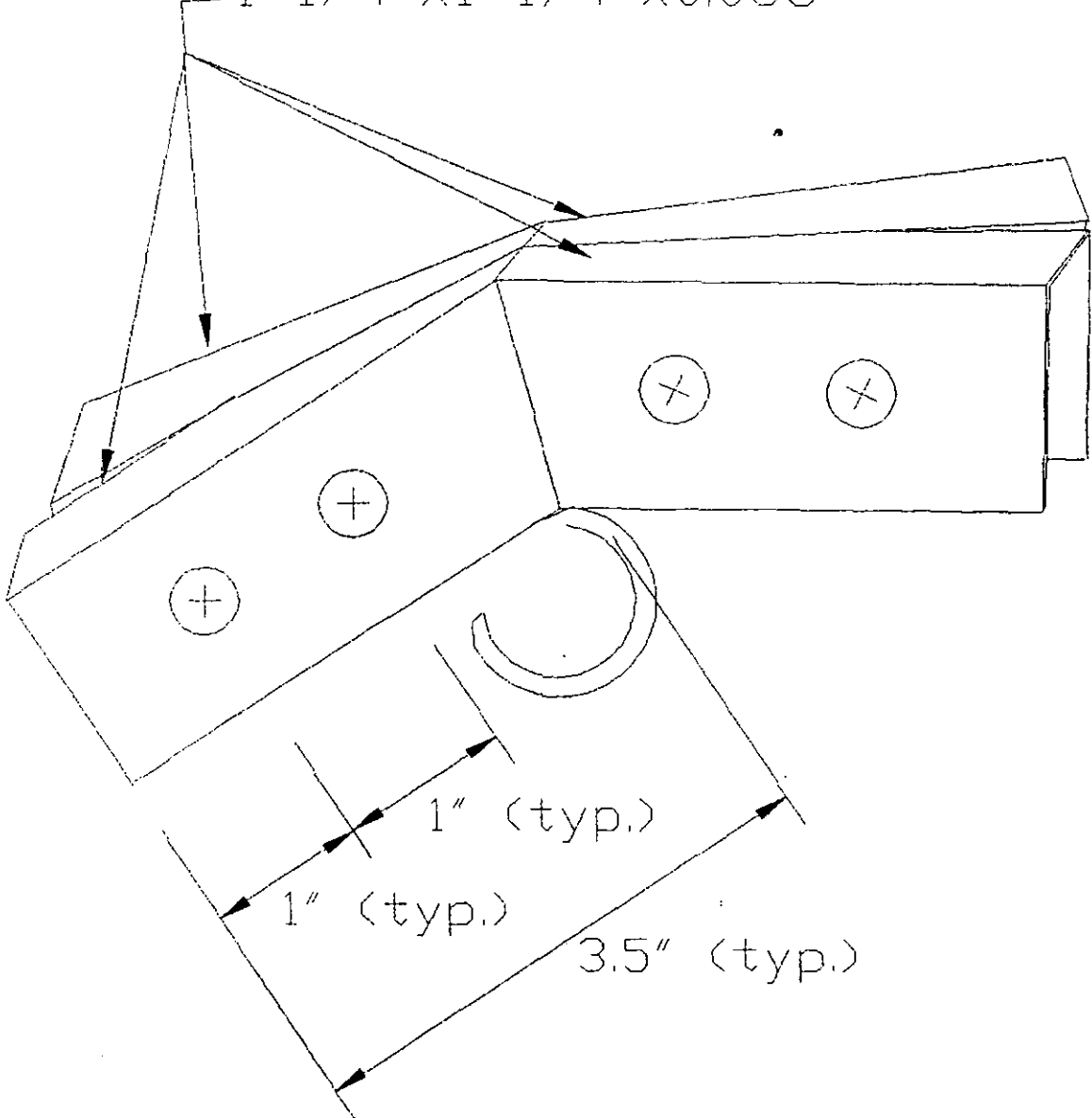
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Team #6		SEC Reference #DES.06.S95	
Client:		EA Reference #:	
Egyptian Associates		BRIDGE06.S95	
Title: Bottom Center Connections (Joints #3, 11)			
Drawn by:	Rachel Davis		Scale: 1"=1"
Date: 4/25/95	Drawing Number: 206		Rev. 0

C-16



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Rev	Date	By	Purpose
SALUKI ENGINEERING COMPANY			
Team #6		SEC Reference #DES.06.S95	
Client: Egyptian Associates		EA Reference #: BRIDGE06.S95	
Title: Top Outer Connections (Joints #6, 8, 14, 15)			
Drawn by: Rachel Davis		Scale: 1" = 1"	
Date: 4/25/95	Drawing Number: 207		Rev 0

1-1/4" x 1-1/4" x 0.083"



3			
2			
1			
Rev	Date	By	Purpose
SALUKI ENGINEERING COMPANY			
Team #6		SEC Reference #DES.06.S95	
Client: Egyptian Associates		EA Reference #: BRIDGE06.S95	
Title: Top Center Connection (Joint #7)			
Drawn by: Rachel Davis		Scale: 1"=1	
Date: 4/25/95	Drawing Number:		Rev
	208		0

BIBLIOGRAPHY

American Institute of Steel Construction, Inc. Manual of Steel Construction: Load and Resistance Factor Design., 1986.

Kassimali, Aslam. Structural Analysis. Computer Software. Boston: PWS Kent Publishing Company, 1993.

SECTION D

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302 Hinged Rods 5, 6, 17, 18	D-11
303 Hinged Rods 11, 12, 23, 24	D-12
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INTRODUCTION

The fabrication process is an important step in the design of the steel bridge. Each step of the process has many important decisions which need to be made at the time of fabrication. These decisions will effect the actual duration of fabrication and the quality of the bridge. The decisions will range from which connections to tack before drilling to what is best fit for the connections. Welding, cutting the steel, and drilling the holes require more time than the other steps in the process and are the most important.

The vendors will effect the fabrication process. Availability of the materials at the time of fabrication and when the materials are received could cause changes in the process. Funding will also have an effect on the process duration.

Sizing and drawings of lateral members and web members are also included in this section. The lateral members are designed to take the 100 lb lateral test and help with the stability in the other tests. The web members are in tension when taking the load for the vertical load tests. All members are taken into account in the fabrication process.

TECHNICAL DISCUSSION

Fabrication Process:

The fabrication process consists of 11 steps taking approximately 37 hours. Time is to be volunteered by the members of the Southern Illinois University American Society of Civil Engineers to accomplish these steps. The estimate is for a 4 member crew. The crew number can be increased on some steps such as painting the bridge and cleaning the bridge, but other steps would be more trouble with more people involved. The times are subject to change as directed by the Chairman of the Bridge Committee, ASCE, SIUC.

Steps:

1. Cut the steel into the specified sizes and file the rough edges.(6 hours)
2. Clean the steel with shop cloths.(0.5 hours)
3. Tack weld the connections that are to be welded, unless the connections are too awkward to fit the drill press.(5.5 hours)
4. Drill the holes. Align the connections while drilling. File any drilled holes which may have rough edges.(6 hours)
5. Weld a strong weld in place of the tack weld.(9 hours)
6. Clean the members as welded together with acetone.(1 hour)
7. Assemble the bridge a few times to see how everything fits together.(2 hours)
8. Coat the bridge with primer.(4 hours)
9. Paint the bridge while it is together to avoid any extra unwanted thickness in member connections.(4 hours)
10. Stencil the school name on the bottom chord members after the primary paint is on.. (2 hours)
11. Practice the assembly process.(as directed by the Bridge Committee Chairman)

TECHNICAL DISCUSSION (continued)

Funding:

There is more than one way to receive funding for the bridge. The first is through the Civil Engineering Department. Procedure is to talk to the chairman, Dr. Sami, to see if funding is available. The next procedure is to politely ask from vendors and private parties for donations in return for displaying their company name at the competition. Some professors and some involved people have privately donated to help fund the bridge in past years. Vendors have also donated materials in past years. The last way to fund the bridge is through the Undergraduate Student Government. This procedure must be done during the school year (appendix B). Any of these methods are acceptable, and if they do not work ASCE will fund the bridge with its own finances.

Design of Lateral Members:

The lateral members were designed to withstand a 100 lb load for the lateral test, a 500 lb load plus the weight of the bridge for the first vertical test, and a 2500 lb load plus the weight of the bridge for the final test. A factor of safety was also used when analyzing the member reactions. The members were designed to be tubular steel due to the compression forces which they can develop along with the tensile forces. Members 25 and 26 are 36" long and are 1/2" square tubular steel with a thickness of 0.049" (Drawing 305). Members 35 and 36 are 14.4" long. Although they carry virtually no load, they have the same thickness as members 25 and 26 for symmetry purposes, and are used for stability (Drawing 304). Members 27 through 34 are approximately 64.9" long, with angles on each end to fit the connections. These members are 0.625" square tubing and are all hinged in the middle with a 0.25" bolt (Drawing 306). Each lateral member is to be cut and drilled according to the fabrication process (Section D) and connected as specified in the connection specification (Section C).

* for additional discussion on lateral bracing see Section B.

TECHNICAL DISCUSSION (continued)

Design of Web Members:

The web members were designed to help with stability during the 100 lb lateral load test, withstand a 500 lb load plus the weight of the bridge for the first vertical test, and withstand a 2500 lb load plus the weight of the bridge for the final test. During the analysis the deflection of the members and the bridge was kept to a minimum. A factor of safety was also used when analyzing the member reactions. The members were designed to be threaded steel rods with turnbuckles. Rods were found to be lighter than tubing, but only strong in tension. Since the web members only experience tensile forces we determined to use rods. The turnbuckles are present so the rods can be put into place then tightened for a good fit. Members 37 and 38 are 60" long and have a diameter of 0.375" (Drawing 301). Members 5, 6, 17, 18 are 36" long and have a diameter of 0.25" (Drawing 302). Members 11, 12, 23, 24 are 82.7" long with a hinge in the middle and have a diameter of 0.25" (Drawing 303). Each rod has a turn buckle included in its length which will be used to make the length exact. The rods will be hinged together as specified in the connection specification (Section C).

* for additional discussion on web members see Section B.

MEMBER MATERIALS LIST

ITEM	DIMENSIONS	QTY	LINEAR INCHES*	DESIRED STRENGTH
Structural Steel Tubing (Members 25, 26)	1/2" x 1/2" x 0.049"	2	36.0	Fy = 36 ksi
Structural Steel Tubing (Members 35, 36)	1/2" x 1/2" x 0.049"	2	14.4	Fy = 36 ksi
Structural Steel Tubing (Members 27-34)	5/8" x 5/8" x 0.049"	8	64.9	Fy = 36 ksi
Round Threaded Steel Rods (Members 5, 6, 17, 18)	1/4" diam	4	36.0	Fy = 36 ksi
Round Threaded Steel Rods (Members 11, 12, 23, 24)	1/4" diam	4	82.4	Fy = 36 ksi
Round Threaded Steel Rods (Members 37, 38)	3/8" diam	2	60.0	Fy = 36 ksi
Steel Turnbuckles	1/4" threading	4	-----	325 lb (T)
Steel Turnbuckles	1/4" threading	4	-----	225 lb (T)
Steel Turnbuckles	3/8" threading	2	-----	1000 lb (T)

*These are the exact member lengths. When ordering when cutting the steel, some extra length should be added. It is easy to cut off extra but nearly impossible to lengthen a member which is too short.

EQUIPMENT LIST

All of the needed equipment is available in the SIUC workshop located on the ground floor of Engineering Building D. The equipment in the workshop is as follows:

- 1) Delta Milwaukee drill press
Model # MD 6X110 CW (1/3 hp)
- 2) Emerson 7" horizontal metal cutting band saw
Model # 10-1720T
- 3) Enco vertical band saw
Model # 165-1551
- 4) Tri-star 6" electric bench grinder
- 5) Arc welder
- 6) Power hand drill
- 7) Assorted hand files
- 8) Safety glasses

Note: John Hester is in charge of the workshop and permission must be obtained from him before any work begins. Also, identification cards must be obtained for those students who will be working on the bridge in the workshop during the weekends.

COSTING SUMMARY

Materials:

Structural Steel Tubing:

Type	Length	Quantity	Cost/each	Vendor
1/2" x 1/2" x 0.049	3'	3	\$2.95	TVH
5/8" x 5/8" x 0.049	6'	8	\$6.90	TVH

Vendors:

TVH = True Value Hardware

M-C = McMaster - Carr Supply Company

Round UNC, class 2 Threaded Steel Rods:

Type	Length	Quantity	Cost/each	Vendor
1/4"	3'	8	\$0.96	TVH
1/4"	6'	4	\$1.92	TVH
3/8"	6'	2	\$1.20	TVH

Hook and Eye Steel Turnbuckles (UNC, class 2 threads):

Bolt Diameter	Quantity	Cost/each	Vendor
1/4"	8	\$4.92	M-C
3/8"	2	\$6.87	M-C

Acetone:

Type	Quantity	Cost/each	Vendor
generic	2	\$2.29/pint	TVH

Primer:

Type	Quantity	Cost/each	Vendor
X-O Rust	2	\$3.28/pint	TVH

COSTING SUMMARY (continued)

Paint:

Type	Quantity	Cost/each	Vendor
Spray Enamel	4	\$1.09/12oz	TVH

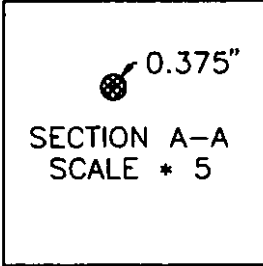
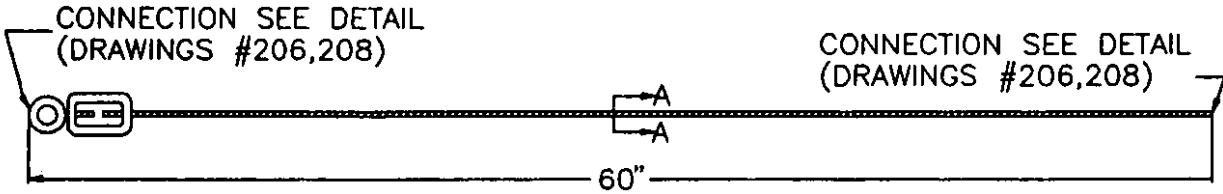
Lubricant:

Type	Quantity	Cost/each	Vendor
WD-40	2	\$1.49/6oz	TVH

Labor and Equipment:

* Since all sections are interdependent this is covered in the Team Section only.

Total Materials Cost = \$153.39



B-10



3			
2			
1	4-19	SO	Corrections
Rev	Date	By	Purpose
SALUKI ENGINEERING COMPANY			
Team #6		SEC Reference #DES.06.S95	
Client:		EA Reference #:	
Egyptian Associates		BRIDGE06.S95	
Title: Hinged Rods 37,38			
Drawn by: Sarah E. Ohler			Scale: 1:10
Date:	Drawing Number:		Rev.
4-15-95	301		0

D-11

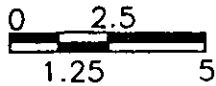
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(DRAWINGS #205,207)

CONNECTION SEE DETAIL
(DRAWINGS #205,207)

36"

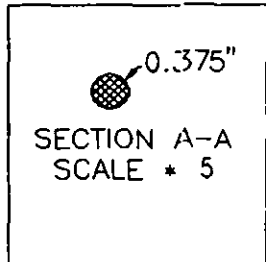
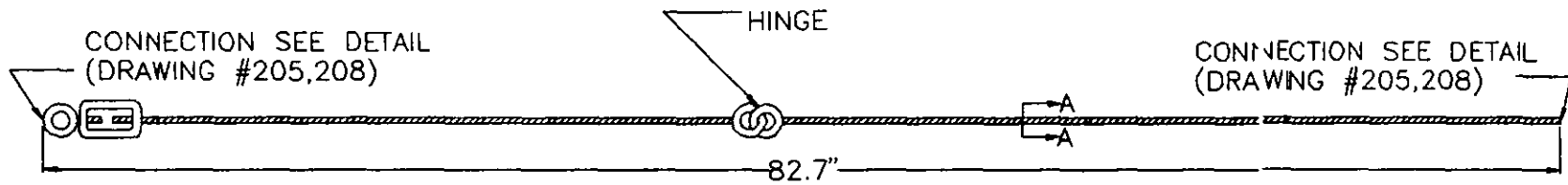
0.25"

SECTION A-A
SCALE * 5



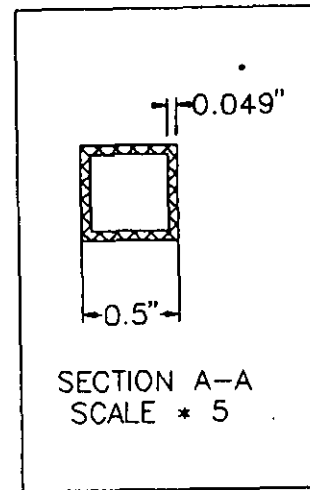
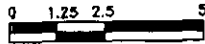
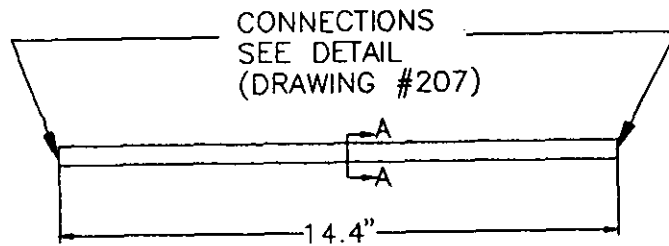
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1	4-15	SO	Corrections
Rev	Date	By	Purpose
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Team #6		SEC Reference #DES.06.S95	
Client:		EA Reference #:	
Egyptian Associates		BRIDGE06.S95	
Title: Hinged Rods 5,6,17,18			
Drawn by: Sarah E. Ohler			Scale: 1:5
Date:	Drawing Number:		Rev.
4-8 -95	302		0

D-12

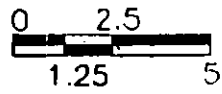
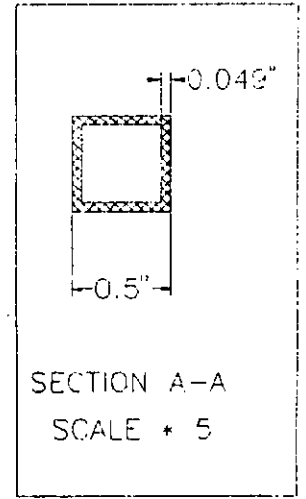
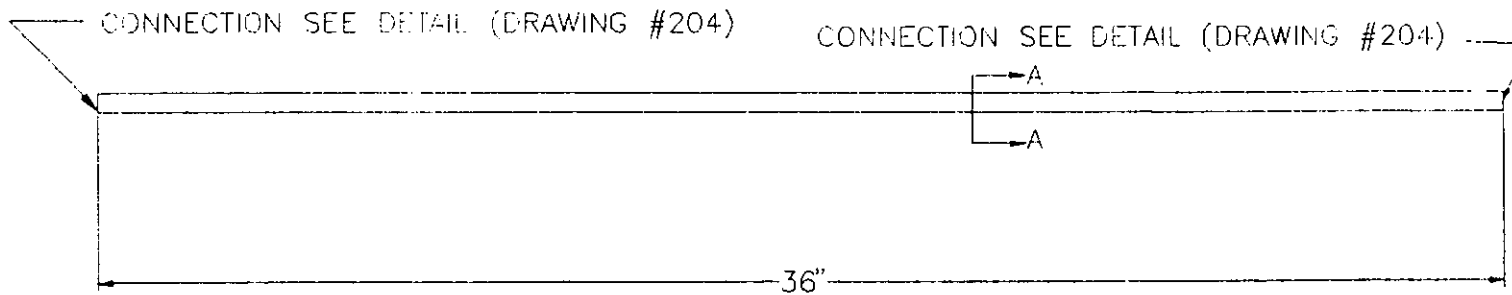


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2	1		
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Rev	Date	By	Purpose
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Team #6		SEC Reference #DES.06.S95	
Client: Egyptian Associates		EA Reference #: BRIDGE06.S95	
Title: Hinged Rods 11,12,23,24			
Drawn by: Sarah E. Ohler			Scale: 1:10
Date: 4-8-95		Drawing Number: 303	
			Rev. 0

D-13



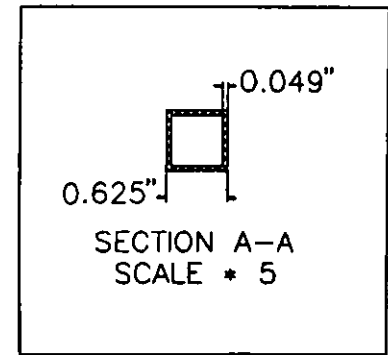
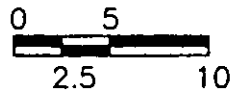
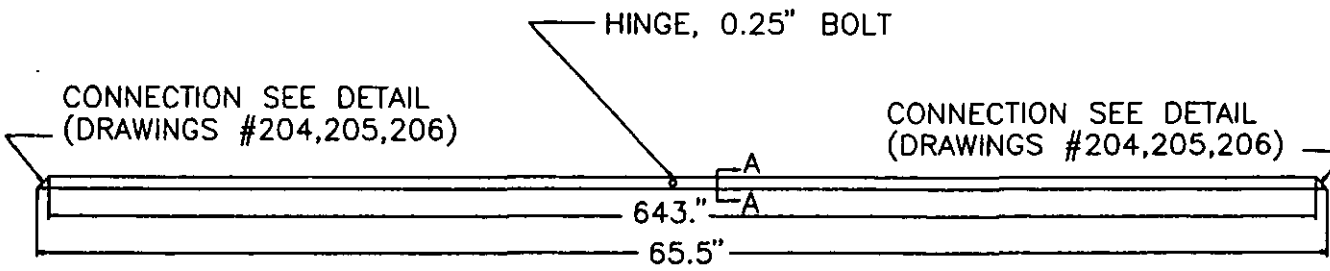
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Client: Egyptian Associates		EA Reference #: BRIDGE06.S95	
Title: Lateral Bracing 35,36			
Drawn by: Sarah E. Ohler		Scale: 1:5	
Date: 4-8-95	Drawing Number: 304		Rev. 0



D-24

3	4-14	SO	Corrections
2	4-8	SO	Corrections
1	4-4	SO	Corrections
Rev	Date	By	Purpose
SALUKI ENGINEERING COMPANY			
Team #6		SEC Reference #DES.06.S95	
Client:		EA Reference #:	
Egyptian Associates		BRIDGE06.S95	
Title: Lateral Bracing 25,26			
Drawn by: Sarah E. Ohler			Scale: 1:5
Date:	Drawing Number:		Rev.
4-3-95	305		0

D-15



3	4-19	SO	Corrections
2	4-15	SO	Corrections
1	4-8	SO	Corrections
Rev	Date	By	Purpose
SALUKI ENGINEERING COMPANY			
Team #6		SEC Reference #DES.06.S95	
Client:		EA Reference #:	
Egyptian Associates		BRIDGE06.S95	
Title: Lateral Bracing 27, 28, 29, 30, 31, 32, 33, 34			
Drawn by: Sarah E. Ohler			Scale: 1:10
Date:	Drawing Number:		Rev.
4-4-95	306		0

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SECTION E

Appendix A:
Final Computer Analysis

```

*****
* .Computer Software *
*   for             *
* STRUCTURAL ANALYSIS *
*   by              *
*   Aslam Kassimali *
*****

```

```

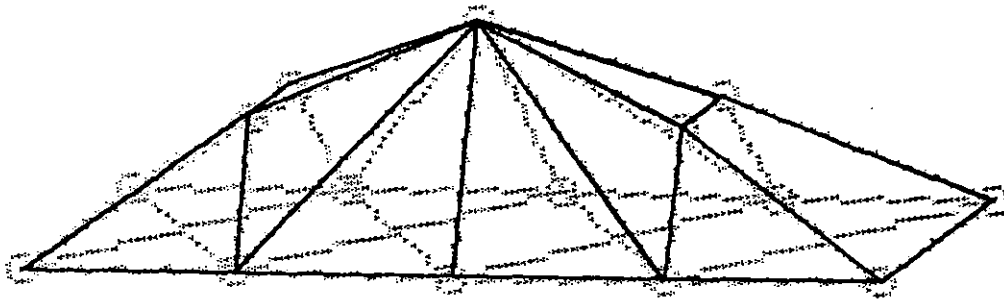
=====
General Structural Data
=====

```

```

Project Title : THE TRUSS
Structure Type : Space Truss
Number of Joints : 15
Number of Members : 38
Number of Material Property Sets (E) : 1
Number of Cross-Sectional Property Sets (A & I) : 1

```



```

=====
Joint Coordinates
=====

```

Joint No.	X Coordinate	Y Coordinate	Z Coordinate
1	+0.0000E+00	+0.0000E+00	+0.0000E+00
2	+5.4000E+01	+0.0000E+00	+0.0000E+00
3	+1.0800E+02	+0.0000E+00	+0.0000E+00
4	+1.6200E+02	+0.0000E+00	+0.0000E+00
5	+2.1600E+02	+0.0000E+00	+0.0000E+00
6	+5.4000E+01	+3.6000E+01	+1.0800E+01
7	+1.0800E+02	+6.0000E+01	+1.8000E+01
8	+1.6200E+02	+3.6000E+01	+1.0800E+01
9	+0.0000E+00	+0.0000E+00	+3.6000E+01
10	+5.4000E+01	+0.0000E+00	+3.6000E+01
11	+1.0800E+02	+0.0000E+00	+3.6000E+01
12	+1.6200E+02	+0.0000E+00	+3.6000E+01
13	+2.1600E+02	+0.0000E+00	+3.6000E+01
14	+5.4000E+01	+3.6000E+01	+2.5200E+01
15	+1.6200E+02	+3.6000E+01	+2.5200E+01

```

=====
Supports
=====

```

Joint No.	X Restraint	Y Restraint	Z Restraint
1	Yes	Yes	Yes
5	No	Yes	No
9	Yes	Yes	Yes
13	No	Yes	No

=====
 Member Data
 =====

Member No.	Beginning Joint	End Joint	Material No.	Cross-Sectional Property No.
1	1	2	1	1
2	2	3	1	1
3	3	4	1	1
4	4	5	1	1
5	2	6	1	1
6	4	8	1	1
7	1	6	1	1
8	5	8	1	1
9	6	7	1	1
10	8	7	1	1
11	2	7	1	1
12	4	7	1	1
13	9	10	1	1
14	10	11	1	1
15	11	12	1	1
16	12	13	1	1
17	10	14	1	1
18	12	15	1	1
19	9	14	1	1
20	13	15	1	1
21	14	7	1	1
22	15	7	1	1
23	10	7	1	1
24	12	7	1	1
25	1	9	1	1
26	5	13	1	1
27	2	9	1	1
28	3	10	1	1
29	4	11	1	1
30	5	12	1	1
31	1	10	1	1
32	2	11	1	1
33	3	12	1	1
34	4	13	1	1
35	14	6	1	1
36	15	8	1	1
37	3	7	1	1
38	11	7	1	1

2500 lb Vertical Test Load

=====
 Joint Loads
 =====

Joint No.	X Force	Y Force	Z Force
2	+0.0000E+00	-3.3125E+02	+0.0000E+00
3	+0.0000E+00	-6.6250E+02	+0.0000E+00
4	+0.0000E+00	-3.3125E+02	+0.0000E+00
10	+0.0000E+00	-3.3125E+02	+0.0000E+00
11	+0.0000E+00	-6.6250E+02	+0.0000E+00
12	+0.0000E+00	-3.3125E+02	+0.0000E+00

=====
 Member Axial Forces
 =====

Note: Positive values are compressive forces

Member No.	Axial Force
1	-9.9773E+02
2	-1.0395E+03
3	-1.0474E+03
4	-9.8977E+02
5	-2.3056E+02
6	-2.3056E+02
7	+1.2108E+03
8	+1.2108E+03
9	+1.0955E+03
10	+1.0955E+03
11	-1.5220E+02
12	-1.5220E+02
13	-9.9773E+02
14	-1.0395E+03
15	-1.0474E+03
16	-9.8977E+02
17	-2.3056E+02
18	-2.3055E+02
19	+1.2108E+03
20	+1.2108E+03
21	+1.0955E+03
22	+1.0955E+03
23	-1.5220E+02
24	-1.5220E+02
25	+0.0000E+00
26	-1.9610E+02
27	+4.7864E+00
28	+1.7437E+02
29	+1.8394E+02
30	-4.7847E+00
31	+4.7856E+00
32	+1.7436E+02
33	+1.8394E+02
34	-4.7853E+00
35	+8.2057E-04
36	+4.1028E-04
37	-6.9167E+02
38	-6.9167E+02

100 lb Lateral Test Load

=====
Joint Loads
=====

Joint No.	X Force	Y Force	Z Force
3	+0.0000E+00	+0.0000E+00	+1.0000E+02

=====
Member Axial Forces
=====

Note: Positive values are compressive forces

Member No.	Axial Force
1	-1.6561E+02
2	-1.0383E+02
3	-4.6172E+01
4	+1.5600E+01
5	+7.0922E+00
6	-7.0922E+00
7	-3.7245E+01
8	+3.7245E+01
9	-3.3699E+01
10	+3.3700E+01
11	-9.3636E+00
12	+9.3635E+00
13	+2.4161E+02
14	+2.7833E+01
15	-2.7826E+01
16	+5.8398E+01
17	-7.0923E+00
18	+7.0921E+00
19	+3.7245E+01
20	-3.7244E+01
21	+3.3700E+01
22	-3.3699E+01
23	+9.3637E+00
24	-9.3637E+00
25	+0.0000E+00
26	+2.4666E+01
27	+3.3447E+01
28	+1.2479E+02
29	+3.3447E+01
30	-5.5489E+01
31	-1.2479E+02
32	-3.3447E+01
33	+5.5488E+01
34	-3.3447E+01
35	+0.0000E+00
36	-2.5643E-05
37	+3.8363E-05
38	+2.0584E-05

Virtual Forces: Vertical

=====
 Joint Loads
 =====

Joint No.	X Force	Y Force	Z Force
3	+0.0000E+00	-1.0000E+00	+0.0000E+00

=====
 Member Axial Forces
 =====

Note: Positive values are compressive forces

Member No.	Axial Force
1	-5.2501E-01
2	-6.7501E-01
3	-6.7500E-01
4	-5.2500E-01
5	-1.7401E-01
6	-1.7401E-01
7	+9.1378E-01
8	+9.1378E-01
9	+8.2681E-01
10	+8.2681E-01
11	+2.2973E-01
12	+2.2973E-01
13	+8.8546E-06
14	-4.4999E-01
15	-4.5000E-01
16	+1.9232E-06
17	-2.6616E-07
18	+4.1317E-07
19	+1.1913E-06
20	-1.4816E-06
21	+1.1711E-06
22	-1.2519E-06
23	+1.9475E-07
24	-5.0287E-07
25	+0.0000E+00
26	-1.2821E-06
27	+1.6747E-06
28	+2.7042E-01
29	+1.3999E-06
30	-2.7042E-01
31	-2.7042E-01
32	-1.1782E-06
33	+2.7041E-01
34	-1.4319E-06
35	+1.0017E-07
36	+7.5125E-08
37	-1.0440E+00
38	+3.6000E-08

Virtual Forces: Lateral

=====
Joint Loads
=====

Joint No.	X Force	Y Force	Z Force
3	+0.0000E+00	+0.0000E+00	+1.0000E+00

=====
Member Axial Forces
=====

Note: Positive values are compressive forces

Member No.	Axial Force
1	-1.6561E+00
2	-1.0383E+00
3	-4.6172E-01
4	+1.5600E-01
5	+7.0922E-02
6	-7.0922E-02
7	-3.7245E-01
8	+3.7245E-01
9	-3.3699E-01
10	+3.3700E-01
11	-9.3636E-02
12	+9.3635E-02
13	+2.4161E+00
14	+2.7833E-01
15	-2.7826E-01
16	+5.8398E-01
17	-7.0923E-02
18	+7.0921E-02
19	+3.7245E-01
20	-3.7244E-01
21	+3.3700E-01
22	-3.3699E-01
23	+9.3637E-02
24	-9.3638E-02
25	+0.0000E+00
26	+2.4666E-01
27	+3.3447E-01
28	+1.2479E+00
29	+3.3447E-01
30	-5.5488E-01
31	-1.2479E+00
32	-3.3447E-01
33	+5.5488E-01
34	-3.3447E-01
35	-4.0067E-07
36	-2.0033E-07
37	+2.1610E-07
38	+5.2073E-07

Determination of Bridge Deflection by the Virtual Work Method
 2500 lb vertical test load

Member	Length, L (in)	Area, A (in ²)	Force, F (lb)	Virtual Force Fv (lb)	Fv(FL/A) (lb ² /in)
1	60.0	0.2354	998	5.25E-01	133547.2
2	54.0	0.2354	1040	6.75E-01	161036.5
3	54.0	0.2354	1047	6.75E-01	162120.4
4	60.0	0.2354	990	5.25E-01	132476.6
5	36.0	0.0276	231	1.74E-01	52427.0
6	36.0	0.0276	231	1.74E-01	52427.0
7	65.8	0.1864	-1211	-9.14E-01	390724.2
8	65.8	0.1864	-1211	-9.14E-01	390724.2
9	55.1	0.1864	-1096	-8.27E-01	267930.3
10	55.1	0.1864	-1096	-8.27E-01	267930.3
11	65.3	0.0884	152	-2.30E-01	-25824.5
12	65.3	0.0884	152	-2.30E-01	-25824.5
13	60.0	0.2354	998	-8.85E-06	-2.3
14	54.0	0.2354	1040	4.50E-01	107357.7
15	54.0	0.2354	1047	4.50E-01	108080.3
16	60.0	0.2354	990	-1.92E-06	-0.5
17	36.0	0.0276	231	2.66E-07	0.1
18	36.0	0.0276	231	-4.13E-07	-0.1
19	65.8	0.1864	-1211	-1.17E-06	0.5
20	65.8	0.1864	-1211	1.48E-06	-0.6
21	55.1	0.1864	-1096	-1.17E-06	0.4
22	55.1	0.1864	-1096	1.25E-06	-0.4
23	65.3	0.0884	1522	-1.95E-07	-0.2
24	65.3	0.0884	1522	5.03E-07	0.6
25	36.0	0.0884	0	0.00E+00	0.0
26	36.0	0.0884	196	1.28E-06	0.1
27	64.9	0.1129	-5	-1.67E-06	0.0
28	64.9	0.1129	-174	-2.70E-01	27006.2
29	64.9	0.1129	-184	-1.40E-06	0.1
30	64.9	0.1129	5	2.70E-01	776.0
31	64.9	0.1129	-5	2.70E-01	-776.0
32	64.9	0.1129	-174	1.18E-06	-0.1
33	64.9	0.1129	-184	-2.70E-01	28659.3
34	64.9	0.1129	5	1.43E-06	0.0
35	14.4	0.0884	0	-1.00E-07	0.0
36	14.4	0.0884	0	-7.50E-08	0.0
37	62.6	0.0491	692	1.04E+00	917555.4
38	62.7	0.0491	692	-3.60E-08	-0.0
Total	-----	-----	-----	-----	3148249.9

$$\text{Deflection} = (3,148,249.9)/(29.0E06) = 0.109$$

$$\text{Vertical Deflection of joint 3} = 0.109 \text{ in}$$

Determination of Bridge Deflection by the Virtual Work Method
 100 lb lateral test load

Member	Length, L (in)	Area, A (in ²)	Force, F (lb)	Virtual Force Fv (lb)	Fv(FL/A) (lb ² /in)
1	60.0	0.2354	166	1.66E+00	70236.2
2	54.0	0.2354	104	1.04E+00	24811.6
3	54.0	0.2354	46	4.62E-01	4875.1
4	60.0	0.2354	-16	-1.56E-01	636.2
5	36.0	0.0276	-7	-7.09E-02	647.3
6	36.0	0.0276	7	7.09E-02	647.3
7	65.8	0.1864	37	3.72E-01	4858.8
8	65.8	0.1864	-37	-3.72E-01	4858.8
9	55.1	0.1864	34	3.37E-01	3387.0
10	55.1	0.1864	-34	-3.37E-01	3387.0
11	65.3	0.0884	9	9.36E-02	622.3
12	65.3	0.0884	-9	-9.36E-02	622.3
13	60.0	0.2354	-242	-2.42E+00	149271.0
14	54.0	0.2354	-28	-2.78E-01	1785.6
15	54.0	0.2354	28	2.78E-01	1785.6
16	60.0	0.2354	-58	-5.84E-01	8633.5
17	36.0	0.0276	7	7.09E-02	647.3
18	36.0	0.0276	-7	-7.09E-02	647.3
19	65.8	0.1864	-37	-3.72E-01	4858.8
20	65.8	0.1864	37	3.72E-01	4858.8
21	55.1	0.1864	-34	-3.37E-01	3387.0
22	55.1	0.1864	34	3.37E-01	3387.0
23	65.3	0.0884	-9	-9.36E-02	622.3
24	65.3	0.0884	9	9.36E-02	622.3
25	36.0	0.0884	0	0.00E+00	0.0
26	36.0	0.0884	-25	-2.47E-01	2514.7
27	64.9	0.1129	-33	-3.34E-01	6335.9
28	64.9	0.1129	-125	-1.25E+00	89819.5
29	64.9	0.1129	-33	-3.34E-01	6335.9
30	64.9	0.1129	55	5.55E-01	17547.1
31	64.9	0.1129	125	1.25E+00	89819.5
32	64.9	0.1129	33	3.34E-01	6335.9
33	64.9	0.1129	-55	-5.55E-01	17547.1
34	64.9	0.1129	33	3.34E-01	6335.9
35	14.4	0.0884	0	4.01E-07	0.0
36	14.4	0.0884	0	2.00E-07	0.0
37	62.6	0.0491	0	-2.16E-07	0.0
38	62.7	0.0491	0	-5.21E-07	0.0
Total	-----	-----	-----	-----	542688.1

$$\text{Deflection} = (542,688.1)/(29.0E06) = 0.019$$

$$\text{Lateral Deflection of joint 3} = 0.019 \text{ in}$$

Appendix B:
USG Funding Procedure

USG General Funding

Funding Guidelines for Allocating Student Activity Fees

The following criteria shall be established as the official Finance Committee Policy in determining funding recommendations to the SIUC Student Senate.

- 1) The activity shall meet all State and University regulations regarding the event and its funding by USG.
- 2) The majority of the members of the organizations must be undergraduates, or be a program of interest to undergraduates. (Interest to students is to be determined by the Finance Committee or recommendations from the Senate members.)
- 3) The activity should be of a nature that would be available to all students, not just those belonging to that organization. (Priority given to members.)
- 4) The amount of students participating in the activity should be proportionate to the size of the group, in order to merit the funding request.
- 5) A high degree of student control of the activity is essential in the programming, planning, and implementation of the event.
- 6) The past accountability of the organizations:
 - a. organization's past programming
 - b. involvement of students in the organization
 - c. degree of success programs have had in the past

The considerations will be based on an "After Action Report" submitted by the organization to the Finance Committee within 14 days of the event funded.

- 7) The activity should relate to past activities of the organization to the goals and objectives of the organization as stated in its constitution.

Group Requirements for Funding Consideration

- 1) Groups must be Registered Student Organizations (RSO's) as defined by the Office of Student Development.
- 2) The RSO must be in good standing as defined by the Office of Student Development.
- 3) The RSO must be in good standing as defined by Undergraduate Student Government.
 - a. USG must have a current copy of the RSO's constitution.
 - b. USG must have a current membership list including phone numbers.
 - c. USG must have a current list of officers including phone numbers.
 - d. USG must have an After Action report from the RSO's last funded event.
- 4) The RSO must have a fiscal advisor located within the Office of Student Development.

Travel

Monies will be allocated for travel where members of the organization will:

Represent SIUC and thereby enhance the prestige of the University by proper actions of that organization.

- 2) In the event that an organization is allocated monies, a memorandum summarizing aspects of the program and knowledge gained is to be submitted to the USG Finance Committee within 14 days upon returning to SIUC. Along with an "After Action Report" which can be obtained from Steve Harris in the Office of Student Development.

- Noncompliance with any of the above regulations will be taken into consideration by the Finance Committee for future funding requests.

Transportation

Transportation shall not exceed 50% per event and must be channeled through SIUC Travel whenever possible.

Lodging

Funding for lodging shall not exceed \$30.00 per room per night, nor exceed one week's duration.

Registration

Registration funding shall not exceed 25% of cost. Honorariums shall not exceed 25% of cost.

Conditions for General Funding

- 1) General Funding includes only one-time events such as trips, speakers, rallies, or new programs.
- 2) RSO's are eligible for a maximum of \$7500 per RSO per semester.
- 3) RSO's must have independently raised 50% or more of the amount for which they are asking. First requests for General Funding without fundraising may be given a maximum of \$200 if the need is shown.
- 4) RSO's must show verification of the independently raised monies.
- 5) RSO's may request funding no more than 2 times per semester.
- 6) Priority One RSO's may not receive General Funding.

Items That Will Not Be Funded

- 1) Food and beverages
- 2) Charitable contributions
- 3) No funding "after the fact" (if the Finance Committee has already met.)
- 4) Prizes
- 5) Advertising not for a specific scheduled event that qualifies for General Funding.
- 6) Any items to be budgeted out of Yearly Fee Allocations.

Exceptions to these guidelines may be granted depending on the request, even if it meets the aforementioned guidelines. Any exceptions to the aforementioned guidelines will be granted only in special circumstances when approved by the Finance Committee and a majority of the members present at the regular Student Senate meeting. Special considerations and/or exceptions to the aforementioned guidelines must be agreed on by 2/3 of the Finance Committee. In addition, an expressed written explanation for the special consideration and/or exception must accompany the Bill to Fund before the regular Student Senate meeting.

Appendix C:
Vendor Backup

**True Value Hardware
Vendor Backup**

All three group members went to True Value Hardware in the Murdale Shopping Center and wrote down prices for the materials needed. These items listed below are the prices current and materials available as of April 23, 1995.

Structural Steel Tubing:

Type	Length	Cost/each
1/2" x 1/2" x 0.049	3'	\$2.95
5/8" x 5/8" x 0.049	6'	\$6.90
1" x 1" x 0.049	6'	\$10.69
1 1/4" x 1 1/4" x 0.049	6'	\$12.59
1 1/4" x 1 1/4" x 0.083	6'	\$13.79

Round UNC, class 2 Threaded Steel Rods:

Type	Length	Cost/each
1/4"	3'	\$0.96
1/4"	6'	\$1.92
3/8"	6'	\$1.20

Dent Ring Pins:

Type	Cost/each
1/4" x 1 3/4"	\$2.00

Elevator Bolts:

Type	Cost/each
1/4" x 2"	\$0.32

Acetone:

Type	Cost/each
generic	\$2.29/pint

**True Value Hardware
Vendor Backup (continued)**

Primer:

Type	Cost/each
X-O Rust	\$3.28/pint

Paint:

Type	Cost/each
Spray Enamel	\$1.09/12oz

Lubricant:

Type	Cost/each
WD-40	\$1.49/6oz

Hinges:

Type	Cost/each
1" loose pin	\$2.55/2

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CABLE

MACARCO

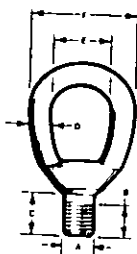
PLANT LOCATION

Elmhurst, Illinois, U.S.A.

MAIL ADDRESS

P.O. Box 4355
Chicago, Illinois 60680, U.S.A.

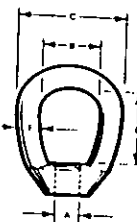
Hoist Rings & Eyes



Drop Forged Lifting Eyes

Forged carbon steel, galvanized finish. Unified National Coarse (UNC) Class 2A threads.

Thread Dia., In. (A)	B	C	D	E	F	Work Limit, l
5/16	1/4	1 1/16	1/4	3/4	1 1/4	
3/8	5/16	1 1/8	3/8	1	1 5/8	
1/2	1/2	1 3/2	1/2	1 1/4	2	
5/8	5/8	1 7/8	5/8	1 1/2	2 1/2	
3/4	3/4	1 7/8	3/4	1 3/4	3	
7/8	7/8	1 7/8	7/8	2	3 1/2	
1	1	2	1	2 1/4	4	
1 1/8	1 1/8	2 1/8	1 1/8	2 1/2	4 1/2	

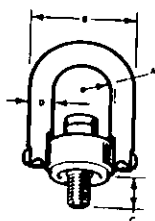


Drop Forged Eye Nuts

Available in galvanized steel and 18-8 type 303 stainless steel. Tapped with Unified National Coarse (UNC) Class 2-B threads.

Note: Loads shown apply to eye nuts only, based on a vertical pull, and not to any connecting bolt or stud.

Thread Dia., In. (A)	B	C	D	E	Work Limit, l	No.	NET EACH
1/4	3/4	1 1/4	1 1/8	1/4	52		
5/16	3/4	1 1/4	1 1/8	3/8	84		
3/8	1	1 1/2	1 1/4	5/8	124		
7/16	1 1/4	2	1 1/2	3/4	170		
1/2	1 1/2	2 1/2	1 1/2	1	224		
5/8	1 1/2	2 1/2	1 1/2	1 1/2	360		
3/4	1 3/4	3	2 3/8	1 1/2	520		
7/8	2	3 1/2	2 3/8	1 3/4	720		
1	2 1/4	4	3 1/8	2	1000		
1 1/8	2 1/4	4	3 1/8	2 1/4	12300	3019T24	112
1 1/4	2 1/2	4 1/2	3 1/2	2 1/2	15500	3019T25	146
1 1/2	3 1/8	5 1/4	4	3	22500	3019T27	285
2	4	7	6 1/4	4 1/2	40000	3019T28	640
303 STAINLESS STEEL							
1/4	3/4	1 1/4	1 1/8	1/4	460	3061T14	\$12.1
5/16	3/4	1 1/4	1 1/8	3/8	780	3061T15	12.1
3/8	1	1 1/2	1 1/4	5/8	1160	3061T17	14.35
1/2	1 1/4	2	1 1/2	1	2150	3061T18	14.35
5/8	1 1/2	2 1/2	1 1/2	1 1/4	3440	3061T21	17.25
3/4	1 3/4	3	2 3/8	1 1/2	5140	3061T23	30.5



Heavy Duty Safety Hoist Rings

Pivots 180° and swivels 360° to compensate for pitch, roll and sway when lifting heavy, unbalanced loads. Reduces risks in lifting, moving and turning heavy machinery, tooling, dies, and other equipment. Alloy steel construction with a corrosion resistant finish. Load ratings are for lifts in any direction.

Bolt Size	Work Load Limit Lbs.	Thread Torque Ft. Lbs.	Dimensions, In.				No.	NET EACH
			A	B	C	D		
5/8"-18	800	7	7/16	1 1/8	3/8	3/8	3052T55	\$ 70.25
3/4"-16	1000	12	7/16	1 1/8	3/8	3/8	3052T56	70.25
1/2"-13	2500	28	1 1/8	2 1/8	1 1/8	1/2	3052T57	85.84
5/8"-11	2500	28	7/8	3 1/4	3/4	3/4	3052T58	85.84
3/4"-11	4000	60	7/8	3 1/4	1	3/4	3052T59	88.44
3/4"-10	5000	100	7/8	3 1/4	1 1/4	3/4	3052T61	88.44
3/4"-10	5000	100	7/8	3 1/4	1	3/4	3052T62	88.44
3/4"-10	7000	100	1 1/8	4 1/8	1 1/2	3/4	3052T63	88.44
7/8"-9	8000	160	1 1/8	4 1/8	1	1	3052T64	185.68
1"-8	10000	230	1 1/8	4 1/8	1	1	3052T65	186.81
1"-8	10000	230	1 1/8	4 1/8	1 1/4	1	3052T66	188.89
1 1/4"-7	15000	470	1 3/4	6	1 1/2	1	3052T67	188.89
2"-4 1/2	30000	800	2 1/4	8	2 1/4	1 1/4	3052T68	344.18
2 1/2"-4	50000	2100	3	10 1/2	4 1/8	1 3/4	3052T69	528.52
3"-4	75000	4300	3 3/4	13	5 3/8	2 1/4	3052T70	1360.65
							3052T71	2277.82



Clevis Eyebolts

Used for heavy lifting operations. Suited for die work and lifting in the construction industry. Rugged shackle pivots on heavy pin; lifting is on a direct plane for smoother motion and stress elimination.

Made of high quality alloy steel. Unified National Coarse (UNC) threads.

Shank, In.	Eye Length, In.	Less Stud	Capacity	No.	NET EACH
1/2-13	1 1/2	4 1/8	1 1/2 tons	3026T14	\$66.92
5/8-11	2 1/8	4 3/8	2 tons	3026T15	71.67
3/4-10	2 1/2	5 1/8	3 1/4 tons	3026T16	86.25
7/8-9	3	6 1/8	4 1/4 tons	3026T17	117.50
1-8	3 1/2	7 1/8	6 1/2 tons	3026T18	142.32
1 1/4-7	4 1/2	8 1/8	8 1/2 tons	3026T19	179.82
1 1/2-6	5	10 1/8	12 tons	3026T21	226.43
2"-4 1/2	6 1/2	16 3/8	25 tons	3026T22	420.62

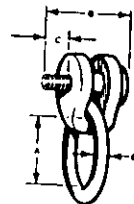


Swivel Lifting Plates

For temporary attachment to steel, wood or construction materials using machine bolt, lag screw or coil bolt. Made of forged steel welded to heavy steel bearing plate. Shackle is forged of 1" diameter stock, and swings on a line through center of bolt.

Maximum Work Load Limit: 9000 lbs., except 1 1/2" size, 12,000 lbs.

Bolt Hole Dia. x Ht.	Plate Size Thk. x W x D	Recommended Minimum Bolt Length	No.	NET EACH
1" x 1 1/8"	1/2" x 2 1/2" x 5"	4"	3070T21	\$57.14
1 1/2" x 2 1/2"	1/2" x 3" x 6"	5"	3070T23	59.26
		6"	3070T25	168.42



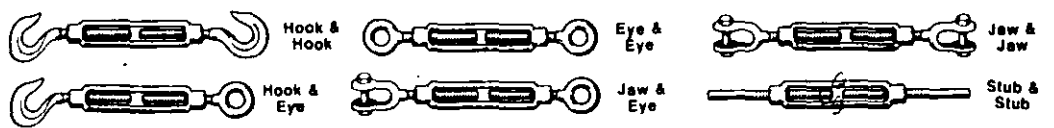
Swivel Hoist Rings

Well suited for industrial lifting applications—dies, fixtures, molds, machinery. Constructed of alloy steel. Clevis, ring, bushing and cap screw are magnetic particle inspected. Bolts have Unified National Coarse Class 3A threads.

Bolt Size In.	Work Load Limit, Lbs.	Thread Torque Ft. Lbs.	Dimensions, In.				No.	NET EACH
			A	B	C	D		
5/16	650	3.5	2	2 1/8	5/8	3/8	8887T62	\$53.77
3/8	800	4.5	2	2 3/8	3/4	3/8	8887T63	56.68
1/2	1800	15.0	3	3 3/8	1	3/8	8887T64	83.09
5/8	2500	25.0	3	3 3/8	1 1/4	5/8	8887T65	85.95
3/4	4100	50.0	4	5	1 1/2	1	8887T66	163.92
1	7100	90.0	4	5 3/8	2	1	8887T67	187.00
1 1/4	14000	150.0	6	6 7/8	2	1 1/4	8887T68	409.00
1 1/2	17200	250.0	6	7 7/8	2 1/2	1 3/8	8887T69	455.67
2	29000	300.0	10	10 1/2	3 1/8	1 1/2	8887T71	646.27

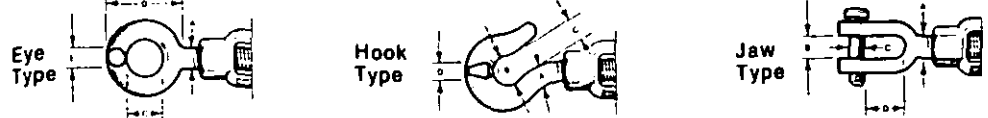
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Turnbuckles



Drop Forged Steel Turnbuckles

Galvanized finish. Meet Federal Specification FF-T-791b, Type 1, Form 1. Jaw type ends are furnished with round pins and coller keys. Bolts have Unified National Coarse (UNC) threads, Class 2. Sizes up to 2 1/2" available—Prices on Request.



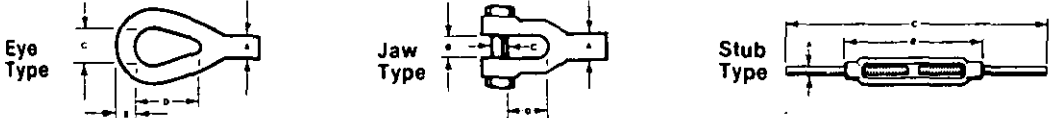
Dimensions, in.				Work Load Limit, Lbs. ♦	Dimensions, in.				Work Load Limit, Lbs. ♦	Dimensions, in.				Work Load Limit, Lbs. ♦
A	B	C	D		A	B	C	D		A	B	C	D	
1/4	1/2	1	1 1/2	500	1/4	3/8	1/2	3/4	400	1/4	3/8	1/2	3/4	500
3/8	1/2	1 1/4	2	800	3/8	1/2	3/4	1	700	3/8	1/2	3/4	1	800
1/2	3/4	1 1/2	2 1/2	1200	1/2	3/4	1	1 1/4	900	1/2	3/4	1	1 1/4	1200
3/4	1	2	3 1/2	2200	3/4	1	1 1/4	2 1/4	1300	3/4	1	1 1/4	2 1/4	2200
1	1 1/4	2 1/4	4 1/4	3500	1	1 1/4	2 1/4	3 1/4	2200	1	1 1/4	2 1/4	3 1/4	3500
1 1/4	1 3/4	3 1/4	5 1/4	5200	1 1/4	1 3/4	3 1/4	4 1/4	2700	1 1/4	1 3/4	3 1/4	4 1/4	5200
1 3/4	2	3 3/4	6 1/4	7000	1 3/4	2	3 3/4	5 1/4	3200	1 3/4	2	3 3/4	5 1/4	7000
2	2 1/4	4 1/4	7 1/4	9800	2	2 1/4	4 1/4	6 1/4	4200	2	2 1/4	4 1/4	6 1/4	9800

♦ Do not exceed working load limit. On hook & eye turnbuckles do not exceed the working load limit shown for the hook end.

Take	Hook & Hook	Hook & Eye	Eye & Eye	Jaw & Eye	Jaw & Jaw
Di.	No.	No.	No.	No.	No.
1/4"	2997T51	2998T51	2999T51	3000T51	3001T51
3/8"	2997T52	2998T52	2999T52	3000T52	3001T52
1/2"	2997T53	2998T53	2999T53	3000T53	3001T53
3/4"	2997T54	2998T54	2999T54	3000T54	3001T54
1"	2997T55	2998T55	2999T55	3000T55	3001T55
1 1/4"	2997T56	2998T56	2999T56	3000T56	3001T56
1 3/4"	2997T57	2998T57	2999T57	3000T57	3001T57
2"	2997T58	2998T58	2999T58	3000T58	3001T58
2 1/4"	2997T59	2998T59	2999T59	3000T59	3001T59
2 3/4"	2997T61	2998T61	2999T61	3000T61	3001T61
3"	2997T62	2998T62	2999T62	3000T62	3001T62
3 1/4"	2997T63	2998T63	2999T63	3000T63	3001T63
3 1/2"	2997T64	2998T64	2999T64	3000T64	3001T64
3 3/4"	2997T65	2998T65	2999T65	3000T65	3001T65
4"	2997T66	2998T66	2999T66	3000T66	3001T66
4 1/4"	2997T67	2998T67	2999T67	3000T67	3001T67
4 1/2"	2997T68	2998T68	2999T68	3000T68	3001T68
4 3/4"	2997T69	2998T69	2999T69	3000T69	3001T69
5"	2997T71	2998T71	2999T71	3000T71	3001T71
5 1/4"	2997T72	2998T72	2999T72	3000T72	3001T72

Drop Forged Stainless Steel Turnbuckles

For applications requiring maximum corrosion resistance, forged from 18-8 Type 303-304 stainless steel. Electro-polished finish. Bolts have Unified National Coarse (UNC) threads. Jaw type ends are furnished with nuts and bolts.



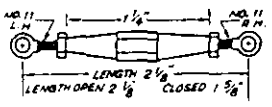
Dimensions, in.				Work Load Limit, Lbs. ♦	Dimensions, in.				Work Load Limit, Lbs. ♦	Dimensions, in.				Work Load Limit, Lbs. ♦
A	B	C	D		A	B	C	D		A	B	C	D	
1/4	1/2	1	1 1/2	460	1/4	3/8	1/2	3/4	460	1/4	3/8	1/2	3/4	460
3/8	1/2	1 1/4	2	780	3/8	1/2	3/4	1	780	3/8	1/2	3/4	1	780
1/2	3/4	1 1/2	2 1/2	1160	1/2	3/4	1	1 1/4	1160	1/2	3/4	1	1 1/4	1160
3/4	1	2	3 1/2	2150	3/4	1	1 1/4	2 1/4	2150	3/4	1	1 1/4	2 1/4	2150
1	1 1/4	2 1/4	4 1/4	3440	1	1 1/4	2 1/4	3 1/4	3440	1	1 1/4	2 1/4	3 1/4	3440
1 1/4	1 3/4	3 1/4	5 1/4	5140	1 1/4	1 3/4	3 1/4	4 1/4	5140	1 1/4	1 3/4	3 1/4	4 1/4	5140
1 3/4	2	3 3/4	6 1/4	7130	1 3/4	2	3 3/4	5 1/4	7130	1 3/4	2	3 3/4	5 1/4	7130
2	2 1/4	4 1/4	7 1/4	9370	2	2 1/4	4 1/4	6 1/4	9370	2	2 1/4	4 1/4	6 1/4	9370

♦ Do not exceed working load limit.

Take	Body Only	Stub & Stub	Eye & Eye	Jaw & Eye	Jaw & Jaw
Di.	No.	No.	No.	No.	No.
1/4"	3022T11	3022T21	3022T31	3022T41	3022T51
3/8"	3022T12	3022T22	3022T32	3022T42	3022T52
1/2"	3022T13	3022T23	3022T33	3022T43	3022T53
3/4"	3022T14	3022T24	3022T34	3022T44	3022T54
1"	3022T15	3022T25	3022T35	3022T45	3022T55
1 1/4"	3022T16	3022T26	3022T36	3022T46	3022T56
1 3/4"	3022T17	3022T27	3022T37		
2"	3022T18	3022T28	3022T38		

Miniature Cable Turnbuckle

Nickel plated brass. For use with miniature coated or uncoated cable. Furnished with one eyebolt and one left hand and one right hand nickel plated brass nut. For cables 1/16" diameter and smaller. No. 3435T12—Pkg. of 5 NET/PKG.\$32.00



Di.	E	F	Wo Lim
1/4	3/4	1 1/4	
3/8	1	1 3/4	
1/2	1 1/4	2	
3/4	1 3/4	2 1/2	
1	2	3 1/2	
1 1/4	2 1/4	4	
1 3/4	2 3/4	4 1/2	

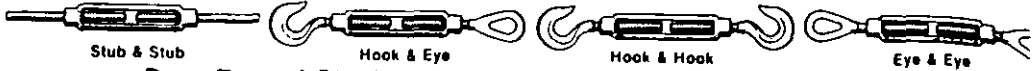
Di.	E	Work L Limit, L	No.	NET EACH
1 1/4"	1/4	52	3019T24	11.50
1 1/4"	1/4	84	3019T25	14.84
1 1/4"	3/8	124	3019T27	28.58
1 1/2"	3/8	170	3019T28	64.00
1 1/2"	1/2	224		
2"	1/2	360		
2 1/4"	3/4	520		
2 3/4"	3/4	720		
3 1/4"	7/8	1000		
3 1/2"	1	12300		
4"	1 1/4	15500		
4 1/2"	1 1/4	22500		
5 1/2"	1 1/2	40000		

Di.	Take	No.	NET EACH
1/4"	4"	2997T51	\$4.92
3/8"	4 1/2"	2997T52	6.17
1/2"	6"	2997T53	6.87
3/4"	6"	2997T54	7.83
1"	9"	2997T55	10.25
1 1/4"	12"	2997T56	12.33
1 3/4"	6"	2997T57	9.97
2"	9"	2997T58	13.80
2 1/4"	12"	2997T59	15.28
2 3/4"	6"	2997T61	17.17
3"	9"	2997T62	19.50
3 1/4"	12"	2997T63	23.10
3 1/2"	18"	2997T64	31.98
3 3/4"	12"	2997T65	28.42
4"	18"	2997T66	41.42
4 1/4"	6"	2997T67	31.67
4 1/2"	12"	2997T68	34.43
4 3/4"	18"	2997T69	52.79
5"	24"	2997T71	62.33
5 1/4"	12"	2997T72	52.50

Di.	Take	No.	NET EACH
1/4"	4"	3022T11	\$9.26
3/8"	4 1/2"	3022T12	12.13
1/2"	6"	3022T13	15.94
3/4"	6"	3022T14	20.38
1"	6"	3022T15	26.29
1 1/4"	6"	3022T16	38.66
1 3/4"	6"	3022T17	41.84
2"	6"	3022T18	54.21

MASTER-CARR

Turnbuckles & U-Bolts



Drop Forged Steel Stub End Turnbuckles

Self-colored finish. Meets Federal Specification FF-T-791b, Type 1, Form 1. Unified National Coarse (UNC) threads. Weldless construction.

Bolt Dia. In.	Take Up In.	Working Load Lbs.	Body Only		Stub & Stub	
			No.	NET EACH	No.	NET EACH
1/4	4	500	2995T14	\$2.05	2996T14	\$3.80
5/16	4 1/2	800	2995T15	2.66	2996T15	4.75
3/8	6	1200	2995T16	2.87	2996T16	5.04
1/2	6	2200	2995T17	3.49	2996T17	6.20
1/2	9	2200	2995T18	5.28	2996T18	8.38
1/2	12	2200	2995T19	5.96	2996T19	10.73
5/8	6	3500	2995T21	3.97	2996T21	6.98
5/8	9	3500	2995T22	5.76	2996T22	10.28
5/8	12	3500	2995T23	6.61	2996T23	11.73
3/4	6	5200	2995T24	5.33	2996T24	9.12
3/4	9	5200	2995T25	6.46	2996T25	11.68
3/4	12	5200	2995T26	9.69	2996T26	16.32
7/8	6	7200	2995T28	6.74	2996T28	12.07
7/8	12	7200	2995T29	10.45	2996T29	21.09
1	6	10000	2995T32	7.99	2996T32	15.01
1	12	10000	2995T33	12.56	2996T33	22.61
1 1/4	6	15200	2995T37	14.39	2996T37	26.87
1 1/4	12	15200	2995T38	17.80	2996T38	34.78
1 1/4	18	15200	2995T39	27.98	2996T39	53.91
1 1/2	6	21400	2995T43	18.75	2996T43	37.47
1 1/2	12	21400	2995T44	26.75	2996T44	49.36

Short Pattern Turnbuckle

Malleable body short turnbuckle has steel swivel bottom assembly. Turnbuckle has right hand threads for top connecting rod. Black finish. Unified National Coarse (UNC) threads.

Bolt Size	Dimensions			Max. Work Load	No.	NET EACH
	A	B	C			
3/8"	3 1/8"	1 9/16"	1 1/2"	610 lbs.	3002T1	\$1.38
1/2"	3 7/8"	1 9/8"	1 3/2"	710 lbs.	3002T2	1.70
5/8"	4 1/8"	2 1/8"	1 7/2"	710 lbs.	3002T3	2.87
3/4"	5 1/4"	2 3/8"	1 9/8"	860 lbs.	3002T4	3.72

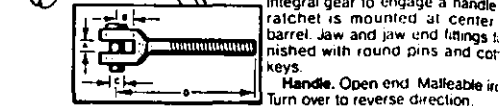
Drop Forged Bronze Turnbuckles

Resists corrosion. National Fine threads provide accurate adjustment. Jaw & Jaw type. Furnished with pins and collars.

Bolt Dia.	Take Up	Min. Length	Max. Length	Wire Dia.	No.	NET EACH
5/16"	3 3/4"	7 1/2"	11 1/4"	1/8" or 5/32"	3011T21	\$3.00
3/8"	4 7/8"	8 3/4"	12 3/8"	3/16"	3011T22	2.87
1/2"	4 7/8"	10"	14 3/8"	1/4" or 9/32"	3011T23	4.75

Heavy Duty Ratchet Turnbuckles

For pipe lines, conveyors & other heavy applications. Cast malleable iron barrels with 3062T and "V" thread design with 3062T Acme thread for extra strength integral gear to engage a handle ratchet is mounted at center barrel. Jaw and jaw end fittings finished with round pins and collars.



TURNBUCKLES

Length	Work Load	Jaw Dimensions				No.	NET EACH	
		A	B	C	D			
18"	26"	5 tons	3/4"	1 1/8"	1/2"	8 1/2"	3062T72	\$5.31
25"	33"	15 tons	1 1/8"	2 1/8"	3/8"	12 3/8"	3062T77	5.87

HANDLES FOR TURNBUCKLES
 For 3062T72 No. 3062T74 NET EACH \$2.20
 For 3062T77 No. 3062T75 NET EACH 4.31

Little Turnbuckles

Zinc plated die cast body. Steel fittings.

Bolt Dia.	Take Up	Lgth. Closed	Eye & Eye		Hook & Hook		NET EACH
			No.	No.	No.	No.	
5/32"	1 1/4"	3 1/4"	3010T14	3010T21	3010T27	3010T28	\$0.72
3/16"	1 1/8"	3 3/4"	3010T15	3010T22	3010T28	3010T29	.72
1/4"	2 3/8"	5 1/2"	3010T17	3010T24	3010T29	3010T31	.96
5/16"	2 3/4"	6 1/2"	3010T18	3010T25	3010T31	3010T32	1.31
3/8"	3"	7 1/2"	3010T19	3010T26	3010T32	3010T32	1.67

Aluminum Alloy Turnbuckles

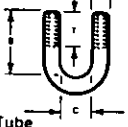
Intended for light duty applications. Cast aluminum body with electrogalvanized steel fittings. Eye fittings not welded. National Coarse Threads. Package of 10.

Bolt Dia.	Length	Eye & Eye		Hook & Hook		NET/PKG.
		No.	No.	No.	No.	
8-32	3 3/8"	4 5/8"	3003T14	3004T14	3005T14	\$5.01
10-24	4"	5 5/8"	3003T15	3004T15	3005T15	5.28
12-24	4 1/2"	6 3/8"	3003T16	3004T16	3005T16	5.78
1/4"-20	5 1/2"	7 5/8"	3003T17	3004T17	3005T17	6.83
5/16"-18	6 3/4"	9 1/4"	3003T18	3004T18	3005T18	11.01
3/8"-16	7 1/2"	10 1/2"	3003T19	3004T19	3005T19	12.70

Aluminum Wrench-Fit Turnbuckles

Flat sides of body fit wrench. Rust resistant extruded aluminum body meets federal strength test specifications. Eyes and hooks are bent, drawn steel wire. Eyes not welded.

Bolt Dia.	Take Up	Eye & Eye		Hook & Hook	
		No.	NET EACH	No.	NET EACH
3/16"	1 5/8"	3038T12	\$0.62		
1/4"	2 1/8"	3038T14	.96		
5/16"	2 3/8"	3038T15	1.23		
3/8"	3"	3038T16	1.82	3038T36	\$1.82



Copper Plated U-Bolts

Lightweight U-bolt is used for the suspension of stationary copper tubing lines. Copper plated steel. Hex nuts not included.

Tube Size	Dimensions				No.	NET EACH
	A	B	C	T		
1/2"	1/4"-20	2 1/4"	1 1/8"	1 1/2"	8882T17	\$0.90
3/4"	1/4"-20	2 1/2"	1 1/8"	1 3/4"	8882T18	.98
1"	1/4"-20	2 3/4"	1 1/8"	1 3/4"	8882T19	1.01
1 1/4"	1/4"-20	3 1/4"	1 3/8"	1 3/4"	8882T21	1.12
1 1/2"	1/4"-20	3 1/4"	1 3/8"	1 3/4"	8882T22	1.19
2"	1/4"-20	3 3/4"	2 1/8"	1 3/4"	8882T23	1.26

Square Bend U-Bolts

For use with channels or other square structural shapes. Zinc plated finish. Unified National Coarse (UNC) threads. Furnish with flat washers and hex nuts.

Thread Dia.	Width Between Legs	Thread Length		No.	NET EACH
		Length	No.		
3/8"	2"	1 1/2"	3060T44	\$1.00	
3/8"	2"	3"	3060T45	1.00	
3/8"	2"	3 3/4"	3060T46	1.00	
3/8"	4"	1 1/2"	3060T47	1.00	
3/8"	4"	3"	3060T48	1.00	
3/8"	4"	3 3/4"	3060T49	1.00	
3/8"	6"	3"	3060T51	1.00	
3/8"	6"	3 3/4"	3060T52	1.00	
3/8"	6"	5 3/8"	3060T53	2.00	

Stainless Steel U-Bolts

Constructed of corrosion resistant Type 304 stainless steel. Furnished with four hex nuts.

For hanging pipe or joists, securing scaffolding and numerous other suspension jobs.

Pipe Size	Dimensions				No.	NET EACH
	A	B	C	T		
1/2"	1/4"-20	2 1/8"	1 1/8"	2 1/2"	8889T41	\$5.20
3/4"	1/4"-20	2 3/8"	1 1/8"	2 1/2"	8889T42	5.50
1"	1/4"-20	2 7/8"	1 1/8"	2 1/2"	8889T43	5.50
1 1/2"	3/8"-16	3 3/4"	1 3/8"	2 1/2"	8889T44	6.00
2"	3/8"-16	4"	1 3/8"	2 1/2"	8889T45	6.20
2 1/2"	1/2"-13	4 1/2"	2 1/8"	2 1/2"	8889T46	6.50
3"	1/2"-13	5 1/4"	3"	3"	8889T47	14.00
3 1/2"	1/2"-13	5 3/8"	3 3/8"	3"	8889T48	15.50
4"	1/2"-13	6 1/8"	4 3/8"	3"	8889T49	19.00

McMASTER-CARR

I D O T - BUREAU OF MATERIALS AND PHYSICAL RESEARCH
 ASSIGNMENT OF MATERIALS 100 THRU 999
 01/01/94 - 12/31/94
 CONTRACT TYPE(S): A L L

YEAR: 94 ===== RPT: MIRC09D

MATL CODE	MATERIAL NAME	PRODUCER NUMBER	PRODUCER NAME	CITY	PROD ST	DIST	P/S	CONTRACT TOTALS STD UNITS	UNASSIGNED QUANTITY STD UNITS
65307501 65307501	SHAPE M270 50W	3484-01	DELONG'S INC.	JEFFERSON CITY	MO	00	S	668.0 668.0	.0 .0
65402	SHAPE ANGLE M183	212-12	BETHLEHEM STEEL CORP	BETHLEHEM	PA	00	PS	12,747.0	.0
65402	SHAPE ANGLE M183	4071-01	BIERBAUM STEEL CO IN	GODFREY	IL	98	S	30,720.0	.0
65402	SHAPE ANGLE M183	436-01	COMMERCIAL FABRICATR	BRIDGEVIEW	IL	91	S	1,023.0	.0
65402	SHAPE ANGLE M183	3484-01	DELONG'S INC.	JEFFERSON CITY	MO	00	S	23,149.0	.0
65402	SHAPE ANGLE M183	846-01	HARTWIG MFG. CORP.	WAUSAU	WI	00	S	43,885.0	.0
65402	SHAPE ANGLE M183	320-01	HENNEGAN & ASSOCIATE	LAGRANGE PARK	IL	91	S	1,826.0	.0
65402	SHAPE ANGLE M183	4838-01	LINCOLN STEEL CO.	LINCOLN	NE	00	S	31,736.0	.0
65402	SHAPE ANGLE M183	1449-01	NORTHWESTERN STL&WIR	STERLING	IL	92	PS	26,936.0	.0
65402	SHAPE ANGLE M183	2394-01	NUCOR CORPORATION	NORFOLK	NE	00	PS	1,395.0	.0
65402	SHAPE ANGLE M183	2186-01	PHOENIX STEEL CORP	EAU CLAIRE	WI	00	S	18,881.0	.0
65402	SHAPE ANGLE M183	3890-01	SMI STEEL INC	BIRMINGHAM	AL	00	PS	1,994.0	.0
65402	SHAPE ANGLE M183	1879-02	STUPP BROS B & I CO	ST LOUIS	MO	98	S	14,366.0	.0
65402	SHAPE ANGLE M183	4007-01	VASQUEZ METAL PROD.	LENZBURG #	IL	98	S	392.0	.0
65402								209,050.0	.0
65405 65405	SHAPE ANGLE M222	3484-01	DELONG'S INC.	JEFFERSON CITY	MO	00	S	8,470.0 8,470.0	.0 .0
6540642 6540642	SHAPE ANGLE M223 42	3484-01	DELONG'S INC.	JEFFERSON CITY	MO	00	S	4,055.0 4,055.0	.0 .0
65407 65407	TEE EXPANSION JOINT	1611-01	J.H. BOTTS, INC.	LEMONT	IL	91	PS	8,883.0 8,883.0	.0 .0
65408 65408	ARMOR ANGLE	3423-01	DREW, JAMES CORP.	INDIANAPOLIS	IN	00	PS	24.0 24.0	.0 .0
6541036 6541036 6541036	SHAPE ANGLE M270 36	2186-01	PHOENIX STEEL CORP	EAU CLAIRE	WI	00	S	1,490.0	.0
	SHAPE ANGLE M270 36	1879-02	STUPP BROS B & I CO	ST LOUIS	MO	98	S	28,381.0	.0
								29,871.0	.0
65411 65411	ARMOR PLATE	1875-01	STRUCT RUBBER PROD	SPRINGFIELD	IL	96	PS	74.0 74.0	.0 .0
65501	BOLT ASTM A325 TY 1	4903-01	DELTA SCREW	CHICAGO	IL	91	S	1,035.0	.0
65501	BOLT ASTM A325 TY 1	2394-05	NUCOR FASTENER CORP	ST. JOE	IN	00	PS	4,617.0	.0
65501	BOLTS ASTM A325 TY 1	1728-01	ST LOUIS SCREW BOLT	ST LOUIS	MO	98	PS	3,117.4	.0
65501	BOLT ASTM A325 TY 1	2010-02	UNYTITE-LOHR	PERU	IL	93	PS	21,628.1	.0
65501								30,397.5	.0
65503 65503 65503	BOLT ASTM A325 TY 3	3484-01	DELONG'S INC.	JEFFERSON CITY	MO	00	S	2,695.8	.0
	BOLTS ASTM A325 TY 3	1728-01	ST LOUIS SCREW BOLT	ST LOUIS	MO	98	PS	27,005.2	.0
								29,701.0	.0

Other Recommended Vendors

F-22

I D O T - BUREAU OF MATERIALS AND PHYSICAL RESEARCH
 ASSIGNMENT OF MATERIALS 100 THRU 999
 01/01/94 - 12/31/94
 CONTRACT TYPE(S): A L L

YEAR: 94 ----- RPT: MIRC09D

MATL CODE	MATERIAL NAME	PRODUCER NUMBER	PRODUCER NAME	CITY	PROD ST	DIST	P/S	CONTRACT TOTALS STD UNITS	UNASSIGNED QUANTITY STD UNITS
6521350	PLATE M270 50	2186-01	PHOENIX STEEL CORP	EAU CLAIRE	WI	00	S	10,793.0	.0
6521350	PLATE M270 50	1879-02	STUPP BROS B & I CO	ST LOUIS	MO	98	S	262,529.0	.0
6521350								1,763,032.0	.0
65213501	PLATE M270 50W	3484-01	DELONG'S INC.	JEFFERSON CITY	MO	00	S	290,326.0	.0
65213501	PLATE M270 50W	846-01	HARTWIG MFG. CORP.	WAUSAU	WI	00	S	773.0	.0
65213501	PLATE M270 50W	4838-01	LINCOLN STEEL CO.	LINCOLN	NE	00	S	19,188.0	.0
65213501	PLATE M270 50W	1879-02	STUPP BROS B & I CO	ST LOUIS	MO	98	S	74,664.0	.0
65213501								384,951.0	.0
65302	SHAPE AASHTO M183	3484-01	DELONG'S INC.	JEFFERSON CITY	MO	00	S	158,136.0	.0
65302	SHAPE AASHTO M183	671-04	FLORIDA STEEL CORP.	JACKSON	TN	00	PS	151.0	.0
65302	SHAPE AASHTO M183	846-01	HARTWIG MFG. CORP.	WAUSAU	WI	00	S	127,900.0	.0
65302	SHAPE AASHTO M183	959-01	INLAND STEEL COMPANY	EAST CHICAGO	IN	00	PS	625.0	.0
65302	SHAPE AASHTO M183	3991-01	ISC	HODGKINS	IL	91	S	8,271.0	.0
65302	SHAPE AASHTO M183	1611-01	J.H. BOTTS, INC.	LEMONT	IL	91	S	255.0	.0
65302	SHAPE AASHTO M183	4838-01	LINCOLN STEEL CO.	LINCOLN	NE	00	S	9,880.0	.0
65302	SHAPE AASHTO M183	1449-01	NORTHWESTERN STL&WIR	STERLING	IL	92	PS	7,519.0	.0
65302	SHAPE AASHTO M183	2186-01	PHOENIX STEEL CORP	EAU CLAIRE	WI	00	S	2,802.0	.0
65302	SHAPE AASHTO M183	1879-02	STUPP BROS B & I CO	ST LOUIS	MO	98	S	3,200.0	.0
65302	SHAPE AASHTO M183	2000-03	UNITED STATES STEEL	SOUTH CHICAGO	IL	91	PS	4,572.0	.0
65302	SHAPE AASHTO M183	4007-01	VASQUEZ METAL PROD.	LENZBURG #	IL	98	S	22,016.0	.0
65302								345,327.0	.0
65305	SHAPE AASHTO M222	212-04	BETHLEHEM STEEL CORP	BURNS HARBOR	IN	00	PS	246,494.0	.0
65305	SHAPE AASHTO M222	3484-01	DELONG'S INC.	JEFFERSON CITY	MO	00	S	176,860.0	.0
65305								423,354.0	.0
6530642	SHAPE AASHTO M223 42	3484-01	DELONG'S INC.	JEFFERSON CITY	MO	00	S	19,405.0	.0
6530642								19,405.0	.0
6530650	SHAPE AASHTO M223 50	3484-01	DELONG'S INC.	JEFFERSON CITY	MO	00	S	242,284.0	.0
6530650	SHAPE AASHTO M223 50	846-01	HARTWIG MFG. CORP.	WAUSAU	WI	00	S	3,368.0	.0
6530650	SHAPE AASHTO M223 50	3991-01	ISC	HODGKINS	IL	91	S	68,046.0	.0
6530650								313,698.0	.0
6530736	SHAPE M270 36	3484-01	DELONG'S INC.	JEFFERSON CITY	MO	00	S	61,161.0	.0
6530736	SHAPE M270 36	4838-01	LINCOLN STEEL CO.	LINCOLN	NE	00	S	24,000.0	.0
6530736	SHAPE M270 36	2186-01	PHOENIX STEEL CORP	EAU CLAIRE	WI	00	S	137,266.0	.0
6530736	SHAPE M270 36	1879-02	STUPP BROS B & I CO	ST LOUIS	MO	98	S	16,500.0	.0
6530736								238,927.0	.0
6530750	SHAPE M270 50	3484-01	DELONG'S INC.	JEFFERSON CITY	MO	00	S	1,069,533.0	.0
6530750	SHAPE M270 50	4838-01	LINCOLN STEEL CO.	LINCOLN	NE	00	S	423,579.0	.0
6530750	SHAPE M270 50	1879-02	STUPP BROS B & I CO	ST LOUIS	MO	98	S	73,163.0	.0
6530750								1,566,275.0	.0

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I D O T - BUREAU OF MATERIALS AND PHYSICAL RESEARCH
ASSIGNMENT OF MATERIALS 100 THRU 999
01/01/94 - 12/31/94
CONTRACT TYPE(S): A L L

YEAR: 94 ===== RPT: MIRC09D

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MATL CODE	MATERIAL NAME	PRODUCER NUMBER	PRODUCER NAME	CITY	PROD ST	DIST	P/S	CONTRACT TOTALS STD UNITS	UNASSIGNED QUANTITY STD UNITS
65202	PLATE AASHTO M183	846-01	HARTWIG MFG. CORP.	WAUSAU	WI	00	S	1,951.0	.0
65202	PLATE AASHTO M183	3517-01	INDIANA STEEL & ENG	BEDFORD	IN	00	S	19,679.0	.0
65202	PLATE AASHTO M183	1611-01	J.H. BOTTS, INC.	LEMONT	IL	91	S	23,999.0	.0
65202	PLATE AASHTO M183	4838-01	LINCOLN STEEL CO.	LINCOLN	NE	00	S	18,196.0	.0
65202	PLATE AASHTO M183	1443-02	NORTH STAR STEEL CO	WILTON	IA	00	PS	44.4	.0
65202	PLATE AASHTO M183	1443-05	NORTH STAR STEEL KY	CALVERT CITY	KY	00	PS	144.0	.0
65202	PLATE AASHTO M183	1449-01	NORTHWESTERN STL&WIR	STERLING	IL	92	PS	57,457.0	.0
65202	PLATE AASHTO M183	2394-01	NUCOR CORPORATION	NORFOLK	NE	00	PS	4,986.0	.0
65202	PLATE AASHTO M183	2186-01	PHOENIX STEEL CORP	EAU CLAIRE	WI	00	S	8,082.0	.0
65202	PLATE AASHTO M183	1879-02	STUPP BROS B & I CO	ST LOUIS	MO	98	S	69,539.0	.0
65202	PLATE AASHTO M183	1400-01	TOBI ENGINEERING INC	GLENVIEW	IL	91	S	2,090.0	.0
65202	PLATE AASHTO M183	2000-05	UNITED STATES STEEL	GARY	IN	00	PS	1,114.0	.0
65202	PLATE AASHTO M183	4007-01	VASQUEZ METAL PROD.	LENZBURG #	IL	98	S	122,141.0	.0
65202								364,015.5	.0
65205	PLATE AASHTO M222	4682-01	CITISTEEL USA	CLAYMONT	DE	00	PS	93.0	.0
65205	PLATE AASHTO M222	3484-01	DELONG'S INC.	JEFFERSON CITY	MO	00	S	4,234.0	.0
65205	PLATE AASHTO M222	1879-02	STUPP BROS B & I CO	ST LOUIS	MO	98	S	2,142.0	.0
65205								6,469.0	.0
6520642	PLATE AASHTO M223 42	3484-01	DELONG'S INC.	JEFFERSON CITY	MO	00	S	2,157.0	.0
6520642	PLATE AASHTO M223 42	1879-02	STUPP BROS B & I CO	ST LOUIS	MO	98	S	4,522.0	.0
6520642								6,679.0	.0
6520650	PLATE AASHTO M223 50	3484-01	DELONG'S INC.	JEFFERSON CITY	MO	00	S	2,505.0	.0
6520650	PLATE AASHTO M223 50	4838-01	LINCOLN STEEL CO.	LINCOLN	NE	00	S	4,896.0	.0
6520650	PLATE AASHTO M223 50	1879-02	STUPP BROS B & I CO	ST LOUIS	MO	98	S	40,443.0	.0
6520650	PLATE AASHTO M223 50	4007-01	VASQUEZ METAL PROD.	LENZBURG #	IL	98	S	2,019.0	.0
6520650								49,863.0	.0
65210	PLATE ASTM A607 GR50	3484-01	DELONG'S INC.	JEFFERSON CITY	MO	00	S	527.0	.0
65210								527.0	.0
65212	PLATE ASTM A606 TY 4	1879-02	STUPP BROS B & I CO	ST LOUIS	MO	98	S	395.0	.0
65212								395.0	.0
6521336	PLATE M270 36	3484-01	DELONG'S INC.	JEFFERSON CITY	MO	00	S	7,218.0	.0
6521336	PLATE M270 36	846-01	HARTWIG MFG. CORP.	WAUSAU	WI	00	S	2,854,626.0	.0
6521336	PLATE M270 36	4838-01	LINCOLN STEEL CO.	LINCOLN	NE	00	S	27,744.0	.0
6521336	PLATE M270 36	2186-01	PHOENIX STEEL CORP	EAU CLAIRE	WI	00	S	59,546.0	.0
6521336	PLATE M270 36	1879-02	STUPP BROS B & I CO	ST LOUIS	MO	98	S	16,208.0	.0
6521336								2,965,342.0	.0
6521350	PLATE M270 50	3484-01	DELONG'S INC.	JEFFERSON CITY	MO	00	S	209,036.0	.0
6521350	PLATE M270 50	846-01	HARTWIG MFG. CORP.	WAUSAU	WI	00	S	1,013,976.0	.0
6521350	PLATE M270 50	4838-01	LINCOLN STEEL CO.	LINCOLN	NE	00	S	266,698.0	.0

I D O T - BUREAU OF MATERIALS AND PHYSICAL RESEARCH
 ASSIGNMENT OF MATERIALS 100 THRU 999
 01/01/94 - 12/31/94
 CONTRACT TYPE(S): A L L

YEAR: 94 ----- RPT: MIRC09D

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MATL CODE	MATERIAL NAME	PRODUCER NUMBER	PRODUCER NAME	CITY	PROD ST	DIST	P/S	CONTRACT TOTALS STD UNITS	UNASSIGNED QUANTITY STD UNITS
63105	STRAND 7WR GR270 LRX	2185-01	AMERICAN SPRING WIRE	BEDFORD HEIGHTS	OH	00	PS	.0	700,943.0
63105	STRAND 7WR GR270 LRX	2210-01	DYWIDAG SYSTEMS	LEMONT	IL	91	S	70,000.0	.0
63105	STRAND 7WR GR270 LRX	2666-01	FLORIDA WIRE-CABLE	JACKSONVILLE	FL	00	PS	.0	84,000.0
63105	STRAND 7WR GR270 LRX	2327-06	INSTEEL WIRE PRODS	GALLATIN	TN	00	PS	.0	84,000.0
63105	STRAND 7WR GR270 LRX	5020-01	PBM CONCRETE INC	ROCHELLE	IL	92	S	.0	171,976.0
63105	STRAND 7WR GR270 LRX	3982-01	RAIDER PRECAST	W. BURLINGTON	IA	00	S	.0	232,580.0
63105								70,000.0	1,273,499.0
63203	BAR SPLICER COUPLER	3989-01	BARSPlice PROD INC	DAYTON	OH	00	PS	108.0	.0
63203	BAR SPLICER COUPLER	3200-01	J & M CONST PRODUCTS	HINSDALE	IL	91	S	512.0	.0
63203	BAR SPLICER COUPLER	2349-01	MATHIS-KELLEY CONST	MORTON	IL	94	S	135.0	.0
63203	BAR SPLICER COUPLER	1650-01	RICHMOND SCR AN	FT. WORTH	TX	00	PS	639.0	.0
63203	BAR SPLICER COUPLER	4518-01	UNIVERSAL REBAR	BELLWOOD	IL	91	PS	1,161.0	350.0
63203								2,555.0	350.0
63204	BAR SPLICE COUP EPXY	3989-01	BARSPlice PROD INC	DAYTON	OH	00	PS	2,370.0	.0
63204	BAR SPLICE COUP EPXY	3131-01	BIRMINGHAM STEEL	BOURBONNAIS	IL	93	PS	16.0	.0
63204	BAR SPLICE COUP EPXY	2177-01	DOWNY B. L. CO.	BROADVIEW	IL	91	S	6,703.0	.0
63204	BAR SPLICE COUP EPXY	2918-01	MIDWEST PIPE COATING	SCHERERVILLE	IN	91	S	2,888.0	.0
63204	BAR SPLICE COUP EPXY	1650-01	RICHMOND SCR AN	FT. WORTH	TX	00	PS	3,345.0	.0
63204	BAR SPLICE COUP EPXY	1650-02	RICHMOND SCR AN	TREMONT	PA	00	PS	5,225.0	.0
63204	BAR SPLICE COUP EPXY	4518-01	UNIVERSAL REBAR	BELLWOOD	IL	91	PS	12,296.0	12,888.0
63204								32,843.0	12,888.0
65102	BAR AASHTO M183	138-01	ATLANTIC STEEL CO.	ATLANTA	GA	00	PS	112.0	.0
65102	BAR AASHTO M183	3131-01	BIRMINGHAM STEEL	BOURBONNAIS	IL	93	PS	494.0	.0
65102	BAR AASHTO M183	3484-01	DELONG'S INC.	JEFFERSON CITY	MO	00	S	11,552.0	.0
65102	BAR AASHTO M183	1611-01	J.H. BOTTS, INC.	LEMONT	IL	91	S	1,982.0	.0
65102	BAR AASHTO M183	4838-01	LINCOLN STEEL CO.	LINCOLN	NE	00	S	2,618.0	.0
65102	BAR AASHTO M183	1449-01	NORTHWESTERN STL&WIR	STERLING	IL	92	PS	45,194.8	.0
65102	BAR AASHTO M183	2394-01	NUCOR CORPORATION	NORFOLK	NE	00	PS	282.5	.0
65102	BAR AASHTO M183	1879-02	STUPP BROS B & I CO	ST LOUIS	MO	98	S	102.0	.0
65102	BAR AASHTO M183	4007-01	VASQUEZ METAL PROD.	LENZBURG	IL	98	S	170.0	.0
65102								62,507.3	.0
65105	BAR AASHTO M222	1443-01	NORTH STAR STEEL CO	ST. PAUL	MN	00	PS	53.0	.0
65105	BAR AASHTO M222	1879-02	STUPP BROS B & I CO	ST LOUIS	MO	98	S	855.0	.0
65105								908.0	.0
6510650	BAR AASHTO M223 50	846-01	HARTWIG MFG. CORP.	WAUSAU	WI	00	S	1,545.0	.0
6510650								1,545.0	.0
65202	PLATE AASHTO M183	138-01	ATLANTIC STEEL CO.	ATLANTA	GA	00	PS	1,598.0	.0
65202	PLATE AASHTO M183	3484-01	DELONG'S INC.	JEFFERSON CITY	MO	00	S	25,334.0	.0
65202	PLATE AASHTO M183	845-01	DREW, P.H., INC.	INDIANAPOLIS	IN	00	S	960.0	.0
65202	PLATE AASHTO M183	4473-01	GENEVA STEEL	PROVO	UT	00	PS	6,701.1	.0

I D O T - BUREAU OF MATERIALS AND PHYSICAL RESEARCH
 ASSIGNMENT OF MATERIALS 100 THRU 999
 01/01/94 - 12/31/94
 CONTRACT TYPE(S): A L L

YEAR: 94 ----- RPT: MIRC09D

MATL CODE	MATERIAL NAME	PRODUCER NUMBER	PRODUCER NAME	CITY	PROD ST	DIST	P/S	CONTRACT TOTALS STD UNITS	UNASSIGNED QUANTITY STD UNITS
65506 65506	ROD THREADED A687	138-01	ATLANTIC STEEL CO.	ATLANTA	GA	00	PS	96.0 96.0	.0 .0
65602	NUT ASTM A194 GR 2H	4903-01	DELTA SCREW	CHICAGO	IL	91	S	389.8	.0
65602	NUT ASTM A194 GR 2H	4744-01	DOMESTIC NUT CORP.	PAINESVILLE	OH	00	PS	.0	1,745.0
65602	NUT ASTM A194 GR 2H	551-01	DYSON CORP.	PAINESVILLE	OH	00	PS	.0	378.0
65602	NUT ASTM A194 GR 2H	1611-01	J.H. BOTTS, INC.	LEMONT	IL	91	S	.0	5,073.1
65602	NUTS ASTM A194 GR 2H	1728-01	ST LOUIS SCREW BOLT	ST LOUIS	MO	98	S	934.1	.0
65602	NUT ASTM A194 GR 2H	2010-02	UNYTITE-LOHR	PERU	IL	93	PS	8,732.0	3,312.5
65602								10,055.9	10,508.6
65606	NUT ASTM A563 GR DH	4744-01	DOMESTIC NUT CORP.	PAINESVILLE	OH	00	PS	.0	3,381.1
65606	NUT ASTM A563 GR DH	1611-01	J.H. BOTTS, INC.	LEMONT	IL	91	S	.0	3,559.1
65606	NUT ASTM A563 GR DH	2394-05	NUCOR FASTENER CORP	ST. JOE	IN	00	PS	1,243.0	.0
65606								1,243.0	6,940.2
65701	WASHER F436 CRBN STL	4903-01	DELTA SCREW	CHICAGO	IL	91	S	2,020.0	.0
65701	WASHER F436 CRBN STL	2394-05	NUCOR FASTENER CORP	ST. JOE	IN	00	PS	102.0	.0
65701	WASHERS A325 TY10R2N	1728-01	ST LOUIS SCREW BOLT	ST LOUIS	MO	98	S	217.5	.0
65701	WASHER F436 CRBN STL	2172-01	WROUGHT WASHER MFG	MILWAUKEE	WI	00	PS	1,656.0	.0
65701								3,995.5	.0
65702	WASHER F436 WTHR STL	3484-01	DELONG'S INC.	JEFFERSON CITY	MO	00	S	310.2	.0
65702	WASHER F436 WTHR STL	1728-01	ST LOUIS SCREW BOLT	ST LOUIS	MO	98	S	2,341.3	.0
65702								2,651.5	.0
65801	CONNECTOR STUDSHEAR	4636-01	A & A ERECTORS	CAMPBELL HILL	IL	99	S	21,861.0	.0
65801	CONNECTOR STUDSHEAR	701-03	FREESSEN, INC.	BLUFFS	IL	96	S	2,900.0	.0
65801	CONNECTOR STUDSHEAR	5067-01	INVENTORY SALES CO.	ST. LOUIS	MO	00	S	168.0	.0
65801	CONNECTOR STUDSHEAR	1611-01	J.H. BOTTS, INC.	LEMONT	IL	91	S	72.0	.0
65801	CONNECTOR STUDSHEAR	1423-01	NELSON STUD WELDING	BRIDGEVIEW	IL	91	S	104,641.0	9,000.0
65801	CONNECTOR STUDSHEAR	1423-02	NELSON STUD WELDING	LORAIN	OH	00	PS	134,500.0	520,340.0
65801	CONNECTOR STUDSHEAR	4392-01	NSS INDUSTRIES	PLYMOUTH	MI	00	PS	5,610.0	.0
65801	CONNECTOR STUDSHEAR	4272-01	POWER FASTENING SUPP	GILBERTS	IL	91	S	101,711.0	229,150.0
65801	CONNECTOR STUDSHEAR	4273-01	STUD WELDING ASSOC.	ELYRIA	OH	00	PS	97,640.0	.0
65801	CONNECTOR STUDSHEAR	4687-01	TOBEK, INC	ST. CHARLES	MO	98	S	12,943.0	.0
65801	CONNECTOR STUDSHEAR	1964-01	TRU-FIT SCREW PDTS	MEDINA	OH	00	PS	103,199.0	18,800.0
65801								585,245.0	777,290.0
67601	BOLT AN GALV STDSPC	99-01	ANCHOR BOLT COMPANY	ST LOUIS	MO	98	PS	8.0	.0
67601	BOLT AN GALV STDSPC	224-02	BBC FASTENERS	ALSIP	IL	91	PS	192.0	100.0
67601	BOLT AN GALV STDSPC	4146-01	BELLEVILLE ELEC SUP	BELLEVILLE	IL	98	S	68.0	.0
67601	BOLT AN GALV STDSPC	4480-01	CENTREX ELEC. SUPPLY	ST. LOUIS	MO	00	S	148.0	.0
67601	BOLT AN GALV STDSPC	2540-01	EGIZII ELECTRIC	SPRINGFIELD	IL	96	S	.0	60.0
67601	BOLT AN GALV STDSPC	2540-03	EGIZII ELECTRIC	DECATUR	IL	95	S	126.0	.0
67601	BOLT AN GALV STDSPC	629-02	FABSCO CORPORATION	CALUMET PARK	IL	91	PS	60.0	16.0

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P = producer
 S = supplier



**SQUARE STRUCTURAL TUBING
CARBON STEEL**

Outside Dimension In Inches	Wall Thickness		Nominal* Inside Dimension in Inches	Weight per Ft. in Lbs.	ASTM A500 GrB UNS K03000		HR Butt Welded
	Ga.	Dec.			ASTM A513		
1/2x	.18	.049	.402	.301		X	
	.063	.063	.374	.363		X	
	.16	.065	.370	.385		X	
5/8x	.18	.049	.527	.384		X	
	.16	.065	.495	.500		X	
	.18	.049	.652	.467		X	
3/4x	.063	.063	.624	.577		X	
	.16	.065	.620	.606		X	
	.11	.120	.510	1.03		X	
7/8x	.16	.065	.745	.716		X	
	.20	.035	.930	.459		X	
	.18	.049	.902	.634		X	
1x	.063	.063	.874	.791		X	
	.16	.065	.870	.827		X	
	.072	.072	.856	.909		X	
	.073	.073	.854	.920		X	
	.14	.083	.834	1.04		X	
	.12	.109	.782	1.32		X	
	.11	.120	.760	1.44		X	
1 1/4 x	.18	.049	1.152	.800		X	
	.063	.063	1.124	1.01		X	
	.16	.065	1.120	1.05		X	
	.072	.072	1.106	1.14		X	
	.14	.083	1.084	1.32		X	
	.090	.090	1.070	1.48		X	
	.11	.120	1.010	1.84		X	
	.10	.134	.982	1.95		X	
	.3/4	.188	.874	2.61		X	X
	.18	.049	1.402	.967		X	
1 1/2 x	.063	.063	1.374	1.22		X	
	.16	.065	1.370	1.27		X	
	.072	.072	1.356	1.38		X	
	.14	.083	1.334	1.60		X	
	.12	.109	1.282	2.06		X	
	.11	.120	1.260	2.25		X	
	.140	.140	1.220	2.49		X	X
	.7	.180	1.140	3.23		X	
	.3/4	.188	1.124	3.23		X	X
	.1/4	.250	1.000	4.11		X	X
1 3/4 x	.14	.083	1.584	1.88		X	
	.11	.120	1.510	2.66		X	
	.1/4	.250	1.250	5.10		X	X
2x	.063	.063	1.874	1.66	X		
	.16	.065	1.870	1.71		X	
	.072	.072	1.856	1.89	X		
	.14	.083	1.834	2.16		X	
	.13	.095	1.810	2.46	X	X	
	.12	1.09	1.782	2.80		X	
	.11	.120	1.760	3.07	X		
	.1/8	.125	1.750	3.12	X		
	.145	.145	1.710	3.51		X	X
	.7	.180	1.640	4.17	X		
(Continued)	.3/4	.188	1.624	4.32†	X		X
	.1/4	.250	1.500	5.41†	X		

*Approximate inside dimensions listed to help develop telescoping requirements. †Weight is for Electric Resistance Welded tubes—slightly less than butt welded tubes.



**SQUARE STRUCTURAL TUBING
CARBON STEEL**

Outside Dimension In Inches	Wall Thickness		Nominal* Inside Dimension in Inches	Weight per Ft. in Lbs.	ASTM A500 GrB UNS K03000		HR Butt Welded
	Ga.	Dec.			ASTM A513		
(Continued)	.16	.065	2.370	2.13		X	
	.14	.083	2.334	2.73		X	
2 1/2 x	.11	.120	2.260	3.78	X		
	.1/8	.125	2.250	3.98	X		
	.141	.141	2.218	4.52	X		
	.7	.180	2.140	5.40	X		
	.3/4	.188	2.124	5.59†	X		X
	.1/4	.250	2.000	7.11†	X		X
	.14	.083	2.834	3.29		X	
3x	.12	.109	2.782	4.29	X		
	.11	.120	2.760	4.58	X		
	.1/8	.125	2.750	4.83	X		
	.7	.180	2.640	6.62	X		
	.3/4	.188	2.624	6.87	X		
3 1/2 x	.1/4	.250	2.500	8.81	X		
	.1/8	.125	3.250	5.68	X		
	.3/4	.188	3.124	8.15	X		
4x	.1/4	.250	3.000	10.51	X		
	.11	.120	3.760	6.22	X		
	.1/8	.125	3.750	6.53	X		
	.7	.180	3.640	9.07	X		
	.3/4	.188	3.624	9.42	X		
4 1/2 x	.1/4	.250	3.500	12.21	X		
	.3/4	.188	3.374	14.83	X		
	.3/8	.375	3.250	17.27	X		
	.1/2	.500	3.000	21.63	X		
	.1/4	.250	4.000	14.21	X		
5x	.7	.180	4.640	11.40	X		
	.3/4	.188	4.626	11.97	X		
	.1/4	.250	4.500	15.62	X		
	.3/4	.188	4.374	19.08	X		
	.3/8	.375	4.250	22.37	X		
6x	.1/2	.500	4.000	28.43	X		
	.7	.180	5.640	13.90	X		
	.3/4	.188	5.640	14.53	X		
	.1/4	.250	5.500	19.02	X		
	.3/4	.188	5.374	23.34	X		
7x	.3/8	.375	5.250	27.48	X		
	.1/2	.500	5.000	35.24	X		
	.3/4	.188	6.626	17.08	X		
	.1/4	.250	6.500	22.42	X		
	.3/4	.188	6.374	27.59	X		
8x	.3/8	.375	6.250	32.58	X		
	.1/2	.500	6.000	42.05	X		
	.1/4	.250	7.500	25.82	X		
	.3/4	.188	7.374	31.84	X		
	.3/8	.375	7.250	37.69	X		
10x	.1/2	.500	7.000	48.85	X		
	.5/8	.625	6.750	59.32	X		
	.1/4	.250	9.500	32.63	X		
	.3/4	.188	9.374	40.35	X		
	.3/8	.375	9.250	47.90	X		
.1/2	.500	9.000	62.46	X			

*Approximate inside dimensions listed to help develop telescoping requirements. †Weight is for Electric Resistance Welded tubes—slightly less than butt welded tubes.

NOTE: Larger sizes up to 24" can be furnished by press brake forming. Call us for your requirements.

DIMENSIONS AND PROPERTIES

	OUTSIDE DIM. (in)	WALL THICK. (in)	INSIDE DIM. (in)	AREA (in ²)	INERTIA (in ⁴)	r=SQRT(I/A) (in)
1/2*	0.5	0.049	0.402	0.088396	0.003032	0.165203
	0.5	0.063	0.374	0.110124	0.003578	0.180249
	0.5	0.065	0.37	0.1131	0.003647	0.17956
5/8*	0.625	0.049	0.527	0.112898	0.006288	0.236
	0.625	0.065	0.495	0.1458	0.007713	0.230154
3/4*	0.75	0.049	0.652	0.137396	0.011308	0.28688
	0.75	0.063	0.624	0.173124	0.013733	0.281643
	0.75	0.065	0.62	0.1781	0.014054	0.280906
	0.75	0.12	0.51	0.3024	0.02073	0.261821
7/8*	0.875	0.065	0.745	0.2106	0.023177	0.331744
1*	1	0.035	0.93	0.1351	0.020996	0.394219
	1	0.049	0.902	0.186396	0.028171	0.388759
	1	0.063	0.874	0.236124	0.034708	0.383392
	1	0.065	0.87	0.2431	0.035592	0.382633
	1	0.072	0.856	0.267264	0.038591	0.379993
	1	0.073	0.854	0.270684	0.039008	0.379618
	1	0.0836	0.834	0.304444	0.043017	0.375894
	1	0.109	0.782	0.388476	0.05217	0.366461
	1	0.12	0.76	0.4224	0.055532	0.362583
	1 1/4*	1.25	0.049	1.152	0.235396	0.056683
1.25		0.063	1.124	0.299124	0.070441	0.485273
1.25		0.065	1.12	0.3081	0.072324	0.484501
1.25		0.072	1.106	0.339264	0.078758	0.481814
1.25		0.083	1.084	0.387444	0.088387	0.477629
1.25		0.09	1.07	0.4176	0.094218	0.474991
1.25		0.12	1.01	0.5424	0.118734	0.463915
1.25		0.134	0.982	0.598176	0.125957	0.458878
1.25		0.188	0.874	0.798624	0.154825	0.440301
1 1/2*	1.5	0.049	1.402	0.284396	0.099908	0.592706
	1.5	0.063	1.374	0.362124	0.124869	0.587216
	1.5	0.065	1.37	0.3731	0.128312	0.586437
	1.5	0.072	1.356	0.411264	0.140129	0.583719
	1.5	0.083	1.334	0.470444	0.157973	0.579479
	1.5	0.109	1.282	0.606476	0.196777	0.569614
	1.5	0.12	1.26	0.6624	0.211836	0.565509
	1.5	0.14	1.22	0.7616	0.237264	0.558152
	1.5	0.18	1.14	0.9504	0.281128	0.543875
	1.5	0.188	1.124	0.986624	0.288865	0.541093
1 3/4*	1.5	0.25	1	1.25	0.338542	0.520416
	1.75	0.083	1.584	0.553444	0.256962	0.681393
	1.75	0.12	1.51	0.7824	0.348338	0.667246
2*	1.75	0.25	1.25	1.5	0.578125	0.620819
	2	0.063	1.874	0.488124	0.305561	0.791195
	2	0.065	1.87	0.5031	0.314308	0.790406
	2	0.072	1.856	0.555264	0.344483	0.787651
	2	0.083	1.834	0.636444	0.390541	0.783345
	2	0.095	1.81	0.7239	0.438931	0.778679
	2	11.09	1.782	0.824476	0.493004	0.773279
	2	0.12	1.76	0.9024	0.53374	0.769069
	2	0.125	1.75	0.9375	0.551758	0.767165
	2	0.145	1.71	1.0759	0.620803	0.759611
	2	0.18	1.64	1.3104	0.730504	0.746637
	2	0.188	1.624	1.362624	0.753687	0.743717
	2	0.25	1.5	1.75	0.911458	0.721688

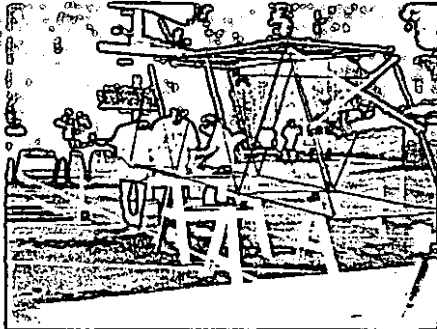
Appendix D:
Combined Bibliography

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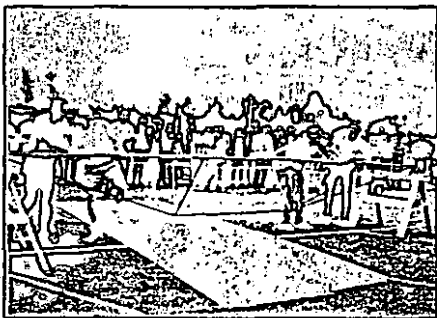
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1995 STEEL BRIDGE BUILDING COMPETITION



*For student chapters of
the American Society
of Civil Engineers*



*In Cooperation With **ASCE**
American Society Of Civil Engineers*

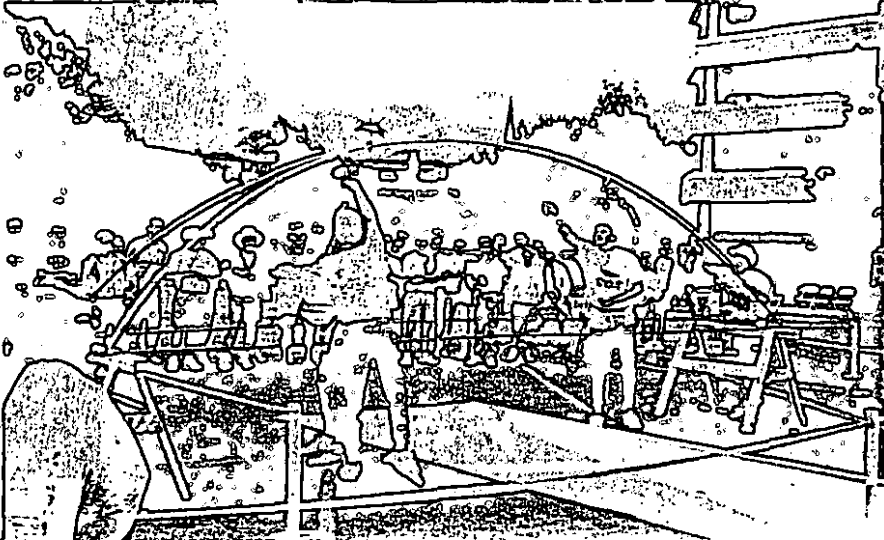
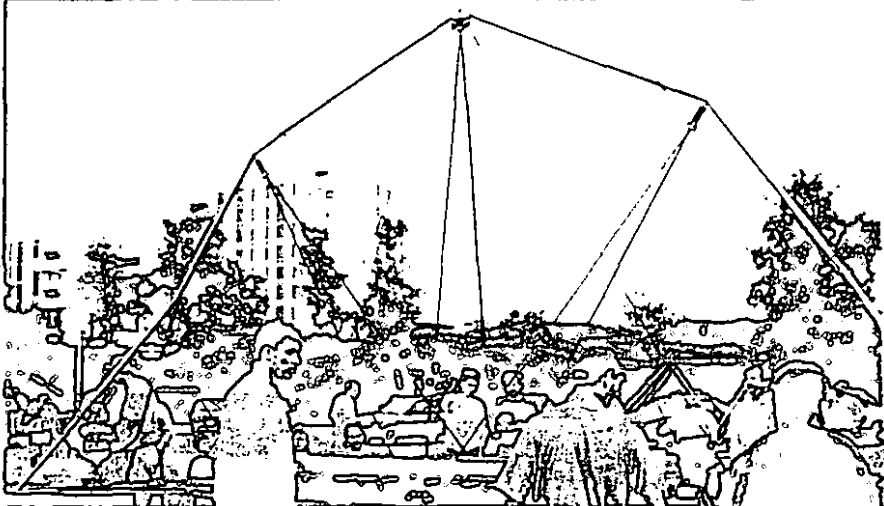
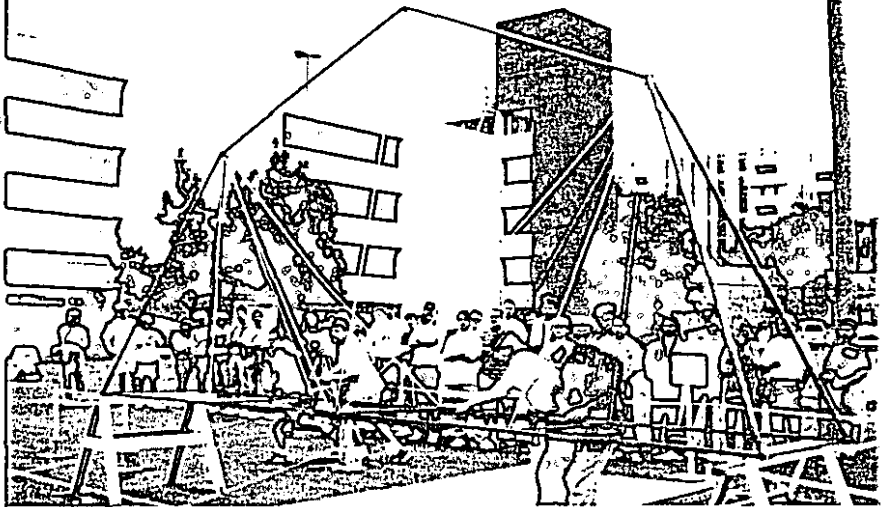
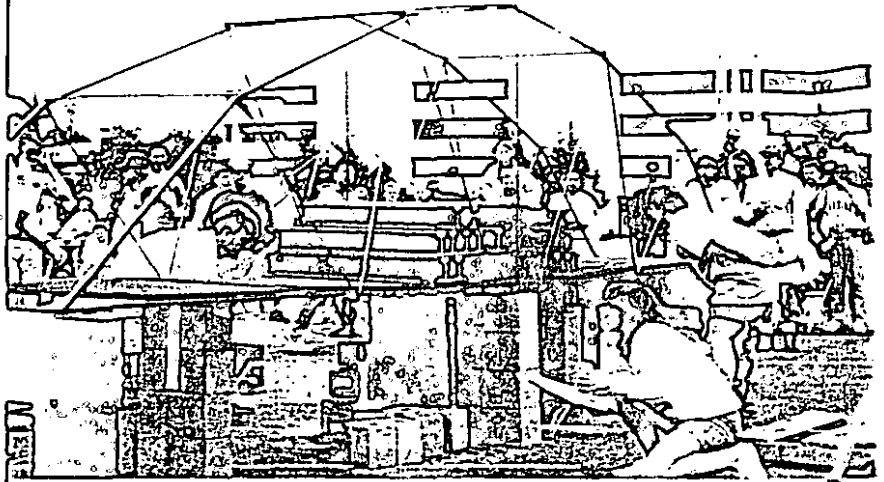


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INTRODUCTION

The Steel Bridge-Building Competition is sponsored by the American Institute of Steel Construction. This inter-collegiate challenge requires Civil Engineering students to design, fabricate and construct a steel bridge.

Safety is of primary importance. The AISC requests that competitors, hosts and judges take all necessary precautions to prevent injury.

The competition rules have been changed for 1995 in order to improve the contest and to assure that competitors design and build new bridges.

Ideally, students should fabricate the entire bridge themselves. However, appropriate shop facilities and supervision may not be available at every college and university. Therefore, the services of a commercial fabricator may be used provided that students observe the operations.

This booklet describes the contest and states the official rules for this year. It is distributed to universities throughout the country. A companion booklet is distributed to hosts and provides directions for conducting a competition.

EXECUTIVE SUMMARY

Civil Engineering students are challenged to an inter-collegiate competition that includes design, fabrication and construction. Participating students gain practical experience in structural design, fabrication processes, construction planning, organization and teamwork.

The Problem Statement describes challenges encountered in a representative structural engineering project. The competition is a scaled simulation of that project.

Standards for durability, constructability, usability, strength and serviceability reflect the volumes of regulations that govern the design and construction of full-scale bridges. Criteria for excellence are represented by the award categories of stiffness, lightness, construction speed, aesthetics, efficiency and economy. As with a real construction project, safety is the primary concern.

The rules of the competition accommodate a large variety of designs and allow innovation. Designers must carefully consider the comparative advantages of various alternatives. For example, a truss bridge may be stiffer than a girder bridge but slower to construct.

The Steel Bridge-Building Competition provides design and construction planning experience, an opportunity to learn fabrication procedures, and the excitement of competing against students from other colleges and universities.

PROBLEM STATEMENT

A century-old bridge that crosses a river valley in a mountainous region must be replaced. The bridge carries heavy truck traffic to and from mines which are the basis for the economy of this rural region, as well as providing access and emergency services to residences. A quick replacement is necessary because no other river crossing of adequate capacity is available for miles.

The State Department of Transportation has requested design/build proposals for replacing the existing bridge. Any appropriate type of bridge will be considered, but the State has specified steel as the material because of its durability and fast erection. The bridge must accommodate two lanes of traffic and be able to carry specified patterns of traffic and wind loads without exceeding deflection limits. In order to expedite environmental approvals, no piers may be erected in the river, nor may temporary scaffolding or causeways be used in the river. However, temporary shoring may be erected on the banks. Construction barges and marine cranes are not feasible due to fast currents and flash floods.

The stone abutments of the existing bridge are in good condition and will serve for the new bridge, provided that no lateral thrust nor uplift is applied to the abutments. The State DOT will not permit modification of the existing abutments. The new bridge, when complete, must be supported only by the existing abutments; for example, stays and anchorages to the river banks are prohibited.

The new bridge must accommodate modular decking, which the State DOT salvaged from another bridge. Decking units may not be modified.

Access to the construction site is limited by narrow, winding roads. This imposes restrictions on the size of components, and on the movements of construction equipment. Soil conditions restrict the weight that may be lifted by cranes.

Your company's design/build proposal is among those that the State DOT has deemed responsive. The DOT has asked each competing firm to submit a 1:10 scale model to demonstrate its concept. Models will be erected under simulated field conditions and then load tested. The DOT will evaluate the models by multiple criteria including durability, constructability, usability, stiffness, construction speed, efficiency, economy and aesthetics. The contract will be awarded to the company that submits the best model. This is an opportunity to become leaders in the bridge replacement market.

QUALIFICATION

In order to compete for awards, a bridge must qualify by satisfying the following minimum standards for durability, constructability, usability, strength and serviceability.

Durability

The bridge must be constructed entirely of steel.

Constructability

The bridge may be constructed only of components conforming to the restrictions on size and weight specified in "Components." The bridge must be constructable according to regulations given in "Construction" and without violating requirements listed in "Safety Regulations."

Usability

The bridge must conform to the specifications described in "Dimensions and Support."

Strength and Serviceability

The bridge must pass load tests 1 and 2 described in "Load Tests."

AWARD COMPETITION

Only qualified bridges are eligible to compete for awards. Categories of competition are stiffness, lightness, construction speed, efficiency, economy and aesthetics. In addition, overall performance is rated.

Stiffness

The bridge with the lowest incremental vertical deflection will win in the stiffness category. Incremental vertical deflection is determined from load test 3. A bridge that fails load test 3 will be eliminated from the stiffness and efficiency categories of competition.

Lightness

The bridge with the least total weight will win in the lightness category. Decking and temporary shoring are not included in total weight.

Construction Speed

The bridge with the lowest construction time will win in this category. Construction time is the product of the size of the construction team and the duration of construction. The construction team includes everyone who handles the bridge or any of its components during timed construction. A bridge that accumulates \$150,000 or more in penalties will be eliminated from competition in the construction speed and economy categories (see "Accidents.")

Efficiency

The bridge with the smallest sum of normalized weight and deflection ratios (SNWD) will win in the efficiency category. The sum of normalized weight and deflection ratios is computed as

$$\text{SNWD} = \frac{\text{Incremental vertical deflection (in)}}{0.20 \text{ (in)}} + \frac{\text{Total weight (lb)}}{100 \text{ (lb)}}$$

Economy

The bridge with the lowest cost (C) will win in the economy category. Cost is computed as

$$\begin{aligned} C = & \text{Total weight (lb)} \times 1000 \text{ (\$/lb)} \\ & + \text{Construction time (person-min)} \times 5000 \text{ (\$/person-minute)} \\ & + \$10,000 \text{ if temporary shoring is used} \\ & + \text{Penalty costs (listed in "Accidents")} \end{aligned}$$

Aesthetics

Factors that may be considered include general appearance, balance and proportion of the design, elegance of connections, finish, construction organization and teamwork. Quality of fabrication should not be considered because some bridges may be fabricated professionally while other are student work.

Overall Performance

The overall performance rating of a bridge is determined by adding the rank of the bridge in the efficiency category to its rank in the economy category. The bridge with the lowest sum will win the overall competition. A bridge that was eliminated from the efficiency and/or economy categories is not eligible for the overall performance competition. In the case of a tie, judges will use aesthetics as the tie breaker.

COMPONENTS

A bridge may be constructed only of components made entirely of steel and conforming to the following descriptions of members, cables with fittings, assemblies, and fasteners.

A member may not weigh more than 40 pounds nor exceed overall dimensions of 5'6" x 7.5" x 7.5." A member may consist of parts connected together before timed construction begins but those parts must remain connected throughout the construction process. A member may be hinged, jointed, articulated or telescoping.

A cable together with its fittings may weigh no more than 40 pounds and must be capable of being coiled to a diameter not exceeding two feet. Fittings are eyes, hooks, plates, clamps, clevises, turnbuckles and similar parts connected to cables, and not exceeding 7.5" in any dimension. A cable with fittings may consist of parts connected together before timed construction begins but those parts must remain connected throughout the construction process. A cable with fittings may have any number of ends.

An assembly is no more than 3 members and/or cables with fittings that are connected together in the staging yards during timed construction.

Fasteners are bolts and nuts, pins, plates, shims and similar parts used for connecting members, cables and assemblies, and not exceeding 7.5" in any dimension.

CONSTRUCTION

Tools

Competitors provide their own tools. Only hand tools are permitted. Field welding and power tools are prohibited. Ropes are permitted but gin poles, jacks, winches, come-alongs, counterweights and other hoisting devices are prohibited. Stools, ladders and similar objects for elevating builders are prohibited.

Construction Site

See the figure titled "Site Plan" for layout of river, banks, and other features that affect construction.

Temporary Shoring

Shoring is temporary support on the river banks, and is provided by the competitors. There are no restrictions on the materials and design for temporary shoring other than it must provide sufficient strength and stability to

support the bridge and builders. There is a cost assigned to temporary shoring; its advantage is that builders may be supported by the bridge only if temporary shoring is in place. If temporary shoring is used, it must be used on both banks.

Safety Support

During construction the top of the safety support must be in place at the midspan of the bridge with its top surface no more than 8 inches from the bottom of the bridge.

Start

Before construction begins, all members, cables with fittings, fasteners, tools and builders are in the staging yards. Temporary shoring, if used, has been constructed and is in place on both river banks. The safety support is in place. Timing and construction begin when the builders signify that they are ready and the judge declares the start.

Time

Time is kept from the start to finish of construction. The clock will be stopped:

1. if a builder or judge sees a condition that could cause personal injury;
2. when a safety regulation has been violated, and
3. if the safety support must be adjusted.

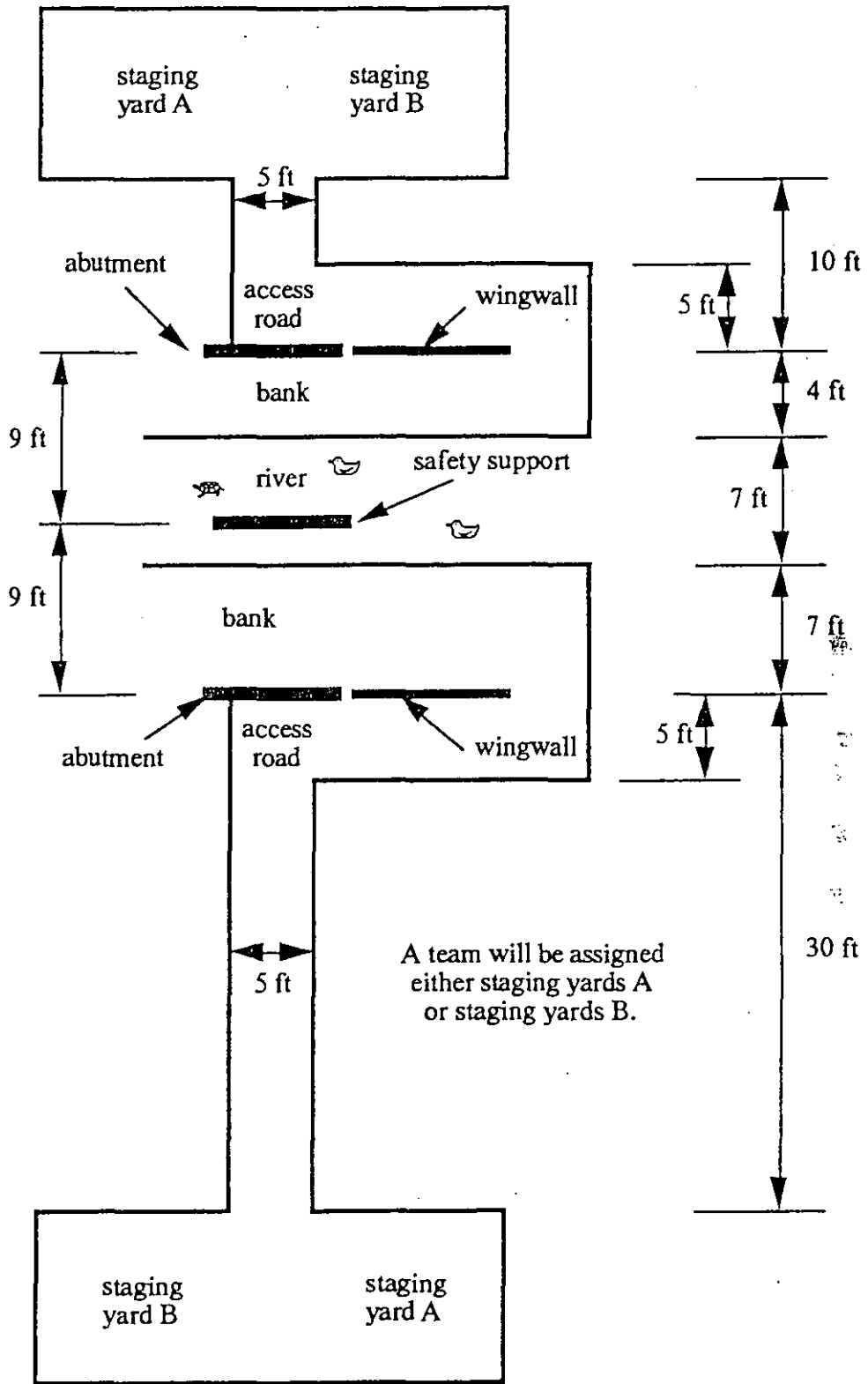
Construction ceases while the clock is stopped. The clock is restarted after the situation has been corrected.

Time Limit

In order to expedite the competition the host may limit the clock time for constructing a bridge to 30 minutes. A higher limit may be imposed. A bridge that exceeds the limit will be eliminated from all categories of competition. If the host opts to impose a time limit, all competitors must be notified at least a month before the competition.

Finish

Construction ends when the bridge is complete, and all tools and builders are in the staging yards, and the builders signify that they are finished. Temporary shoring may remain on the banks. Installation of decking is not included in timed construction.



Site Plan

SAFETY REGULATIONS

If any of the following safety regulations are violated the judge will stop the clock and explain the violation. Before restarting the clock, builders, tools and bridge components will be returned to the positions they occupied before the violation. Construction that necessitates violation of safety regulations is not permitted.

1. If temporary shoring is not used, a builder may not stand on the bridge nor occupy it in any other way such that the bridge supports the builder's body weight. However, a builder may lean on the bridge if both feet remain on the river bank.

2. Temporary shoring may not be placed in the river.

3. A builder may lift or carry only one member or one cable with fittings at a time.

4. An assembly may not be lifted nor carried by one builder alone.

5. Two or more builders may lift or carry only one assembly at a time.

6. Nothing may be thrown.

7. A builder may not stand, sit or kneel in the river, nor use the river for support in any way.

8. A builder must stay within the limits of the access roads and river banks.

9. A builder may not cross the wingwalls.

10. The safety support as well as temporary shoring on both banks must be in place and properly adjusted before a builder climbs onto the bridge.

11. A builder may not cross the abutments except to climb onto the bridge with temporary shoring and safety support in place.

12. No member, cable with fittings nor assembly may be carried while climbing onto the bridge.

13. A builder may not cross the river by jumping, by temporary scaffolding, by crossing the bridge, nor by any other means.

14. A member, cable with fittings, assembly, fastener or tool may not be laid down except in the staging yards, on the abutments, on the temporary shoring and on the bridge. A member, cable with fittings, assembly, fastener or tool may not be leaned against an abutment, temporary shoring or safety support.

15. A constructed portion of the bridge may be slid horizontally, provided that it is supported by both abutments, or by temporary shoring on both banks, or by one abutment and one unit of temporary shoring.

16. One side or end of a constructed portion of the bridge may be moved a few inches in any direction in order to align a connection.

ACCIDENTS

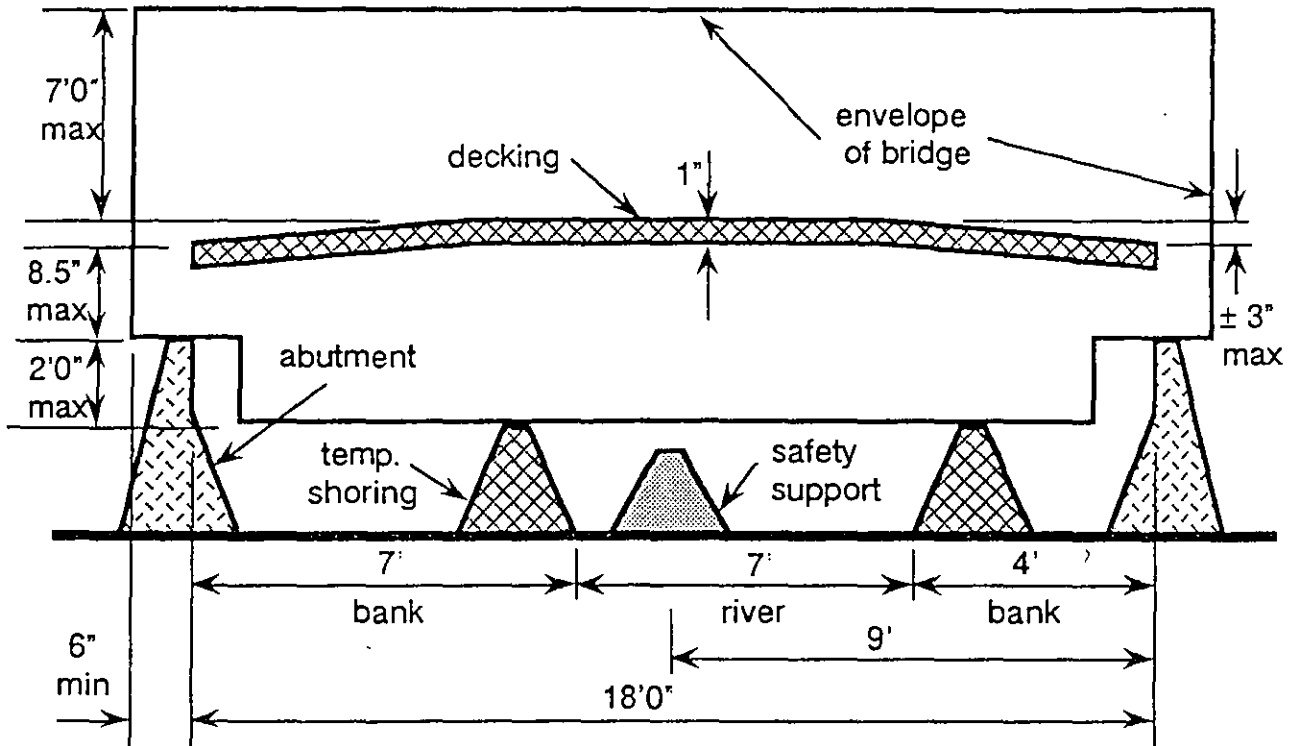
In general, the clock is not stopped when an "accident" occurs. Builders involved in accidents may continue to build, and components involved in accidents may be recovered and used. Types of accidents and the corresponding cost penalties are:

1. A builder touches the river or the safety support. \$50,000 for each occurrence.
2. A member, cable with fittings, assembly, or the bridge touches the river, a bank, an access road or the safety support. \$20,000 for each occurrence.
3. A tool or fastener touches the river, a bank or an access road. \$1000 for each occurrence.

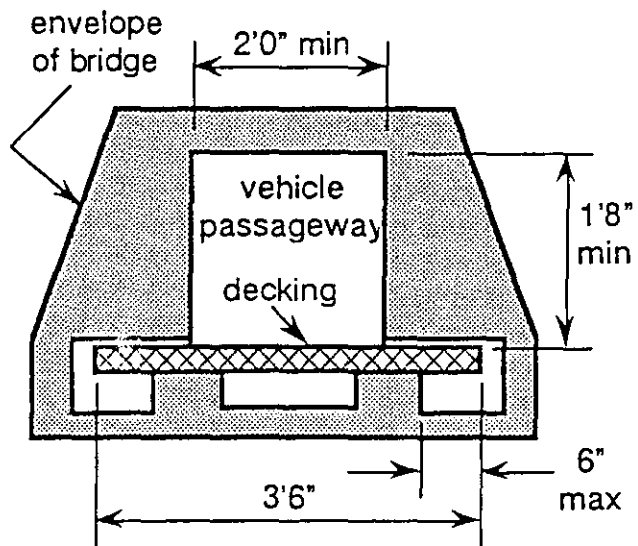
DIMENSIONS AND SUPPORT

The figures titled "Side Elevation" and "Clearance and Deck Support" illustrate some of the following specifications.

1. The bridge must span the abutments, which are fixed in place so that the distance between faces is 18 feet.
2. The bridge must provide bearing area extending at least 6 inches behind the face of each abutment so that the bridge will remain supported by the abutments in the event that it is displaced 6 inches in the direction of span.
3. A 2'0" wide by 1'8" high rectangular vehicle passageway must be provided along the full length of the bridge.
4. No part of the bridge may extend more than 2 feet below the top of the abutments at any point on the span.
5. No part of the bridge may extend more than 7 feet above the top of the deck at any point on the span.



Side Elevation



Clearance and Deck Support

6. The surface of the deck must be no more than 8.5" above the top of the abutments, measured at the abutments.

7. The absolute value of camber must not exceed 3 inches.

8. The bridge must provide support for the decking on both of the edges that run in the longitudinal direction of the bridge. The support must be continuous for the full span of the bridge.

9. The edges of the decking that run in the longitudinal direction of the bridge may be cantilevered over their supports no more than 6 inches.

10. The continuous supports for the deck must be capable of accommodating decking anywhere on the span, without gaps, overlaps or abrupt elevation differences between decking units. However, small elevation differences, such as those caused by decking resting on bolt heads, are acceptable.

11. The decking may not be attached nor anchored to the bridge.

12. The bridge may not be attached nor anchored to the abutments, and it may bear only on the top surface of the abutments.

13. The bridge may not be anchored, tied nor braced to the ground.

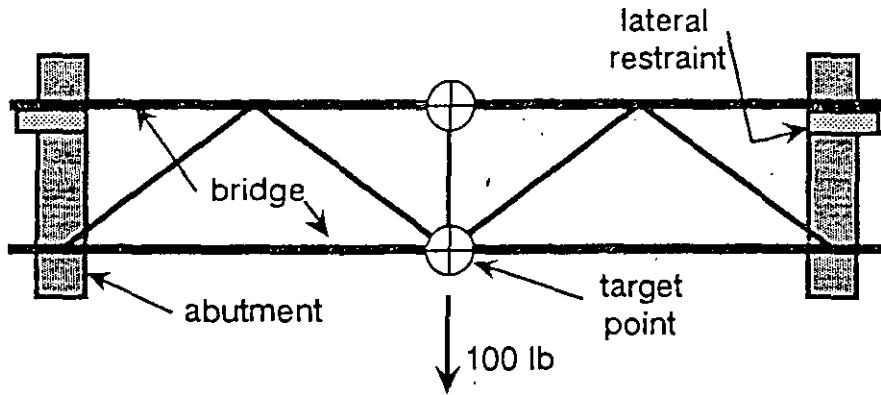
LOAD TESTS

CAUTION: A bridge could collapse or sway suddenly during load tests. Therefore, minimize the number of people near the bridge while it is being tested. During testing the bridge must be supported so that its lowest point is no more than 8 inches above ground or above the top of the safety support.

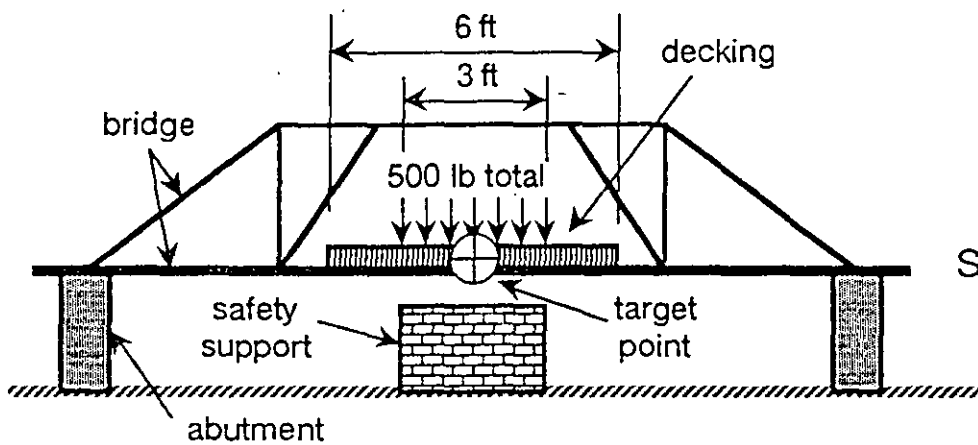
The figure titled "Load Tests" illustrates some of the following procedures.

Load tests are conducted without temporary shoring. Load test 1 is conducted without decking; load tests 2 and 3 are conducted with two decking units installed to accommodate the load.

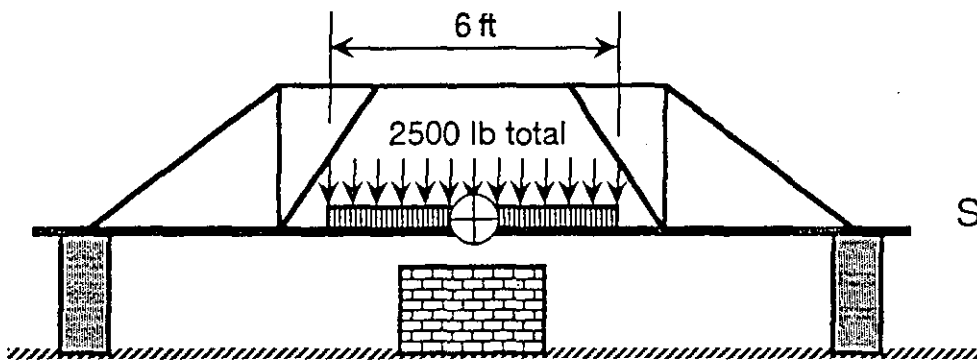
The judge designates two target points on the bridge, both located at midspan, one on each side. The target points should be close to the level of the deck, and may be on the decking itself. Lateral deflection measurements are made to the target point on one side of the bridge, designated by the judge. Vertical deflection measurements are made to both target points; vertical deflection is the maximum absolute value of the two measurements.



Load Test 1
Plan



Load Test 2
Side Elevation



Load Test 3
Side Elevation

Load Tests

Total lateral deflection is the absolute value of the horizontal distance of the target point from its position at the beginning of load test 2. Incremental vertical deflection is the maximum absolute value of the vertical distances of the target points from their positions at the beginning of load test 3.

Load tests are conducted in numerical order.

Load Test 1 - Qualifying, Lateral

Load test 1 is conducted with lateral restraint installed on the abutments to prevent the ends of the bridge from sliding. As close as practical to midspan apply a 100 pound force in the lateral direction. To pass load test 1, the lateral deflection of the bridge must not exceed 1.0". If the bridge does not pass load test 1, do not conduct any other load test. Remove the lateral load; it is not part of the remaining load tests.

Load Test 2 - Qualifying, Vertical

Uniformly distribute load over an area symmetric about the middle of the deck and extending 3 feet in the span direction. Terminate load test 2 when lateral deflection reaches 1.0" or vertical deflection reaches 2.0" or 500 pounds of load has been placed. A bridge passes load test 2 if 500 pounds of load was placed without a deflection limit being exceeded. If the bridge does not pass load test 2, do not conduct any other load test.

Load Test 3 - Competition, Vertical

With the load from test 2 remaining in place, uniformly distribute additional load over an area symmetric about the middle of the deck and extending 6 feet in the span direction. Terminate load test 3 when total lateral deflection reaches 2.0" or incremental vertical deflection reaches 2.0" or 2000 pounds of additional load has been placed. A bridge passes load test 3 if 2000 pounds of additional load was placed without a deflection limit being exceeded. If the bridge passes load test 3, record the incremental vertical deflection.

EQUIPMENT PROVIDED BY HOST CHAPTER

The following equipment will be provided at the contest site by the host. Competitors may wish to acquire similar equipment for use in practice and testing before the competition.

Lateral Load Device

Capable of applying 100 lb force in the horizontal direction.

Measuring Scales and/or Instruments

Load

2500 pounds total. The load should be supplied in uniform increments of size and weight that may be handled safely. When in place, the load should not provide significant stiffness in the longitudinal direction of the bridge. Sections of steel angle of uniform size and length are recommended for load. Sacks of material, containers of liquid, concrete blocks or jacking systems could be used.

Decking

The decking is steel bar grating identified as W-19-4 (1 x 1/8). The dimensions of a piece of grating are 3'6" x 2'11-3/4" x 1". Grating has bending strength only in the direction of the main bars, which are 3'6" long. The grating will be installed with the main bars perpendicular to the length of the bridge, creating a roadway that is 3'6" wide. Therefore, support for the grating must be provided along the edges that are parallel to the length of the bridge. No support is needed for the edges of the grating that are perpendicular to the length of the bridge.

When loading, do not exceed 400 psf uniform load nor 500 pounds concentrated load. Do not load on a cantilevered portion of the grating.

Abutments

The top surface of each abutment should be at least 5 feet long, 3 inches wide, level, smooth, and approximately 3 feet above the ground. Temporary lateral restraints are needed during load test 1.

Safety Support

The safety support is intended to limit the consequences of a bridge collapsing during construction or load tests, but should not come in contact with the bridge unless there is a collapse or excessive deflection. The safety support is placed at the middle of the span and adjusted so that the top of the support is no more than 8 inches from the bottom of the bridge.

The safety support should be placed and adjusted to the proper height before the start of timed construction. At all times during construction the top of the safety support should be within 8 inches of the bottom of the bridge. If the safety support must be adjusted when the bridge is partially constructed, the clock will be stopped while the safety support is positioned. Builders are prohibited from being on the bridge unless the safety support is in place, as well as temporary shoring on both banks.

The safety support must be at least 6 feet wide in the lateral direction of the bridge.

JUDGING

The host will recruit judges. Judges have full authority over conduct of the competition and interpretation of ambiguities in the rules. Judges are empowered to halt any activity that they deem to be hazardous. Decisions, scoring and rating are the sole responsibility of the judges and will be final.

TIPS FOR COMPETITORS

1. Strive for challenging but realistic goals for design and construction. The following statistics from the 1994 National Steel Bridge-Building Competition suggest the levels of performance that are possible. However, when reviewing these statistics keep in mind that the rules and scoring for 1995 differ from those for 1994.

	Winning bridge in category	Winning bridge, overall
Weight (lb)	84.5	117
Construction time (person-minutes)	10.28	28.60
Incremental vertical deflection (inches)	0.195	0.227

2. Start work on the design early, leaving adequate time to procure materials, fabricate the bridge, load test it and practice construction.
3. Design a bridge that may be fabricated, erected and load tested safely.
4. Design a bridge that may be fabricated with available materials, tools and facilities.
5. Allow tolerances for the decking to be slightly larger or smaller than specified. Provide adequate clearances so that the decking may be installed anywhere on the span.
6. When fabricating your bridge, use safe tools, operate them carefully and with adequate supervision.
7. When load testing your bridge before the competition keep it as low to the ground as possible and place safety supports a few inches below the bridge at intervals along the span. This will prevent injury and limit damage to the bridge if it collapses. Keep hands and feet out from under the bridge.
8. Make sure that abutments, safety supports and temporary shoring are strong enough (with a generous factor of safety) and will not tip during construction practice or if the bridge collapses during load testing.

9. Follow all safety regulations and guidelines during construction practice.
10. Don't stand, sit or lie on your bridge unless a safety support and temporary shoring are in place.
11. To expedite the competition have a preset plan for unloading and staging components of your bridge. Before the competition adjust your temporary shoring to conform to the height of the host's abutments. Know in advance the required elevation of the safety support.

SCORE SHEET

Penalties for Accidents

Builder touches river or safety support (\$50,000 each)	\$ _____
Part touches river, bank, road or safety support (\$20,000 each)	\$ _____
Tool or fastener dropped in river, on bank or road (\$1000 each)	\$ _____
TOTAL PENALTIES	\$ _____

Construction Time

_____ builders x _____ min = _____ person-min

Total Weight _____ pounds

Aesthetics

Items that may be considered:

General appearance	Balance and proportion
Finish	Elegance of connections
Construction organization	Teamwork

AESTHETICS SCORE _____

Deflection (incremental vertical, test 3) _____ inches

Efficiency

Total weight (lb) _____ / 100 = _____

Incremental vert. deflect. (in) _____ / 0.02 = + _____

SNWD (add) _____

Cost

Temporary Shoring: \$10,000 if used \$ _____

Const. Time _____ x \$5000 = +\$ _____

Weight _____ x \$1000 = +\$ _____

Total Penalties _____ +\$ _____

TOTAL COST (add) \$ _____

Rank

Construction Speed _____ Efficiency _____

Lightness _____ Economy _____

Stiffness _____ Aesthetics _____

Overall Performance (Efficiency + Economy) = _____

Use aesthetics as tie breaker